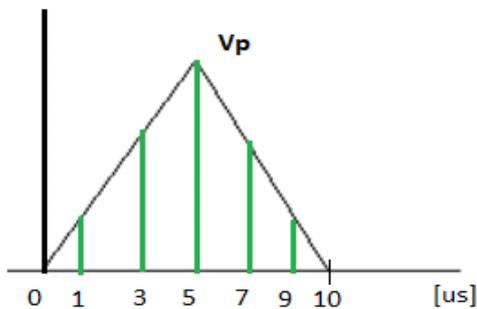


**Problem 1**

- 1) The Fourier transform of the triangular signal is a square sinc with the first zero in  $1/T_p = 1/5\mu s = 200kHz$ . Most of the frequency content of the signal is within 200kHz. To be conservative, we can use a preamplifier with  $f_{pA} = 10 * 200kHz = 2MHz$ . A reasonable value for input referred voltage noise is  $\sqrt{S_V} = 10nV/\sqrt{Hz}$ . Given the preamplifier bandwidth limitation, the output noise has a Lorentzian spectrum with  $\tau = 80ns$ . This time is much lower than the minimum sampling time of the microcontroller so noise samples are always **uncorrelated**. To implement a GI in the digital domain, we must give the same weight to each sample. Exploiting the maximum sampling frequency of the microcontroller, we can acquire 5 samples. To maximize the SNR we must acquire the signal peak, so we must acquire the samples corresponding to the green lines shown in the following figure:



The first half of the signal can be described as follows:

$$S_{ANALOG} = V_p/T_p * t \text{ for } 0 < t < T_p$$

$$S_{DIGITAL} = V_p/T_p * k * T_s/2 \text{ k} \in \{0,1,2,3,4,5\}$$

Therefore, giving the same weight A to all samples we get

$S = V_p/T_p * A * T_s/2 * (1^2 + 3^2 + 5^2)$ , where 1 and 3 have been doubled to take into account the second (descending) part of the signal.

$$N = \sqrt{5 * A^2 * S_v * \frac{\pi}{2} f_{pa}}, \text{ where 5 is the number of acquired samples.}$$

As a result we obtain  $V_{pmin} = 15.2\mu V$ .

- 2) Being able to choose any weight for each sample, we can design a filter that has the same shape of the signal in order to implement a digital version of the optimum filter. In this case the weighting function is equal to 1, 3, 5, 3, 1 for the 5 samples.  
 $S = V_p/T_p * T_s/2 * (1^2 * 2 + 3^2 * 2 + 5^2) = V_p/T_p * T_s/2 * 45$   
 $N = \sqrt{(1^2 * 2 + 3^2 * 2 + 5^2) * S_v * \frac{\pi}{2} f_{pa}}$   
 In this case,  $V_{pmin} = 13.2\mu V$ .
- 3) The digital weighting function tends to its analog counterpart as the sampling frequency tends to infinite. See theory for more details.

## Problem 2

- 1) Wheatstone bridge configuration with 4 Strain Gauges (SGs): 2 SGs are used to collect as much signal as possible, while the remaining 2 are used for temperature compensation (see theory for the placement of the SGs on the component under test).  
With a SG featuring a  $R_0=100\Omega$ , we can use a bias  $V_a=10\text{mV}$  exploiting the whole power budget. A typical Gauge factor  $G$  for the SG is 2.  
The differential signal at the input of the preamp is  $V_a * G/2 * \epsilon$ , where  $\epsilon$  is the applied strain.
- 2) A filter is necessary. Being the signal intrinsically modulated (it's a square wave centered around zero) we can use a LIA. The best solution is demodulating with +/- 1 square wave ( $f_{\text{demod}}=500\text{Hz}$ , duty cycle 50%) and a LPF with  $f_p=10\text{BW}_s = 100\text{Hz}$ . As a result,  $\epsilon_{\text{MIN}} = 5$  microstrain.
- 3)  $1/f$  noise affects the first and the third harmonic of the signal. To minimize its effect we must change the bias of the Wheatstone bridge to modulate the signal, i.e.  $f_a=20\text{kHz}$  to avoid  $1/f$  noise; by using +/- $V_a$  we keep the same power dissipation.  
In this case we need two nested LIAs to extract the signal: the first one with +/-1 demodulation and  $f_{\text{demod}}=20\text{kHz}$  followed by the same acquisition scheme of point b) thus obtaining the same  $\epsilon_{\text{MIN}}$  of point b).