

**Problem 1**

- 1) The minimum detectable signal with the optimum filter (weighting function with the same shape of the signal) is:  $V_{p,MIN} = \sqrt{3S_V/(4T_P)} = 1,55\mu V$ .

A practical suitable filter is the gated integrator. Optimum duration is  $T_G = \frac{4}{3}T_P$ .  $V_{p,MIN} = \sqrt{\frac{S_V}{2} \frac{1}{\sqrt{4/3} T_P * 2/3}} = 1,64\mu V$

- 2) With a periodical signal, the SNR can be improved using a Boxcar. The maximum duration of the Boxcar weighting function must be 1s. The improvement factor is the same for the two cases of point 1) and it is equal to  $\sqrt{2 * \left[\frac{1s}{5} * \frac{T_W}{T_R}\right] * \frac{1}{T_W}} = \sqrt{4000} = 63,2$ .

(Note:  $T_W$  is the duration of the weighting function as in point 1) and  $T_R$  is the inverse of the repetition rate of the signal)

Optimum filter+BI:  $V_{p,MIN} = \frac{1,26\mu V}{63,2} = 19,94nV$

Optimized GI+BI:  $V_{p,MIN} = \frac{1,64\mu V}{63,2} = 25,95nV$

- 3) Both filters discussed in previous points only apply a low pass filtering action on both signal and noise. Therefore, an additional high pass filter is needed to limit 1/f noise. Exploiting all the signal-free interval between pulses to collect only noise, noise doubling is avoided. In this scenario, we compare the contribution of white noise to the one of 1/f noise. Triangular weighting function, with amplitude 1 and duration  $2T_p$ :

- $\sigma_W = \sqrt{\frac{S_V}{2} * T_P} = 6,32\mu V$
- $\sigma_{1/f} \approx \sqrt{S_V f_c \ln\left(\frac{1/T_P}{1/2\pi(T_p+9T_p)}\right)} = 0,364\mu V$

Comment: with the selected filtering option, 1/f noise contribution is negligible with respect to white noise. Therefore, the minimum detectable signal is the same of point 1 and 2. Same considerations hold when a rectangular filtering is applied on the single pulse.

**Problem 2**

- 1) A suitable APD for this application features  $R=0.2$ ,  $w_N$  (neutral region depth) = 200nm,  $w_D$  (depleted region depth) = 5 $\mu m$ ,  $G=100$ ,  $F=2$ , dark current = 20fA. As a result,  $PDE=0.65$ ,  $S_D=0.262A/W$ . The signal can be filtered with a LPF,  $f_p=1kHz$ . The major noise contribution is due to the electronics (amplifier and input resistor). The minimum APD current signal that can be detected with  $SNR=1$  is 63.8pA, which corresponds to  $P_{INC,MIN} = 2.4pW$ .
- 2) Noise would be ideally infinite (practically extremely high) in presence of 1/f noise since no high pass filtering action has been introduced so far. With a zero-setting, in the worst case scenario (acquisition after 2hours),  $I_{APD,MIN} = 198pA$ ,  $P_{INC,MIN} = 7.56pW$ .
- 3) The laser could be modulated on-off, either electrically or by using a mechanical chopper in front of the laser. [Note: a sinusoidal modulation could also be exploited, but the laser has typically a lower power in this mode]. A squarewave +/- 1 LIA is used to demodulate the signal. In this way, the DC component of both signal and noise is removed. After modulation (well above 2kHz to avoid 1/f noise), demodulation and LPF we are in the same scenario of point 1, except for signal power that has been halved. Therefore  $P_{INC,MIN} = 1.2pW$ .