**Sensors, Signals and Noise** 

# COURSE OUTLINE

- Introduction
- Signals and Noise
- Filtering
- Sensors: PD1 PhotoDetector Fundamentals

## Photons and photodetector principles

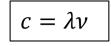
- Photons and Spectral ranges
- Reflection and Absorption of Photons in materials
- Thermal Photodetector Principles
- Quantum Photodetector Principles
- Photon Statistics and Noise
- Current Signals of Quantum Photodetectors

# **Photons and Spectral ranges**

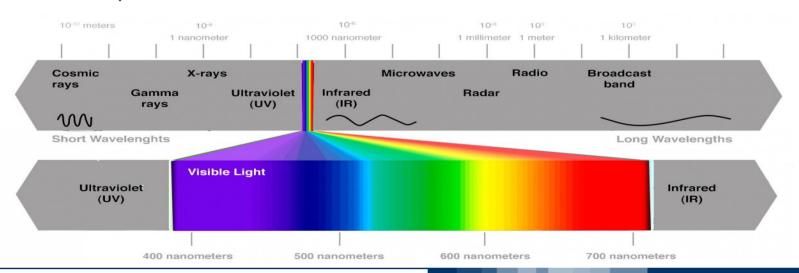
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## **Photons**

- Light = electromagnetic waves with frequency v and wavelength  $\lambda$  propagation speed (in vacuum)  $c = 2,998 \cdot 10^8 \text{ m/s}$
- Spectral ranges:



- $\lambda < 400nm$ Ultraviolet (UV) $400nm < \lambda < 750nm$ **Visible** (VIS) $750nm < \lambda < 3 \mu m$ Near-infrared (NIR) $3 \mu m < \lambda < 30 \mu m$ Mid-infrared (MIR) $30 \mu m < \lambda$ Far-infrared (FIR)
- Energy:  $E_p = hv$  quantum energy (Planck's constant  $h = 6, 6 \cdot 10^{-34} J \cdot s$ )



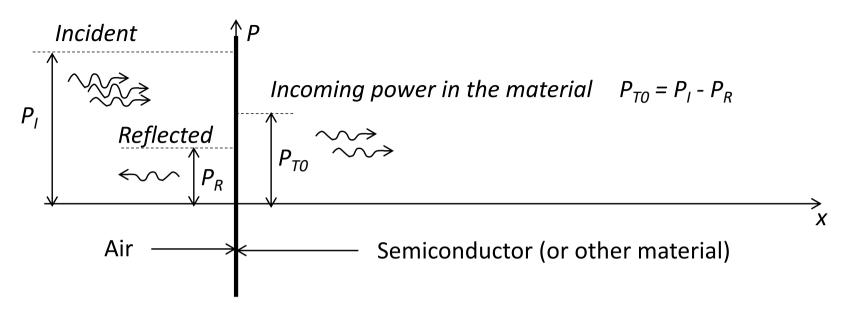
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# **Reflection and Absorption of Photons**

## **Reflection of Photons on the surface**

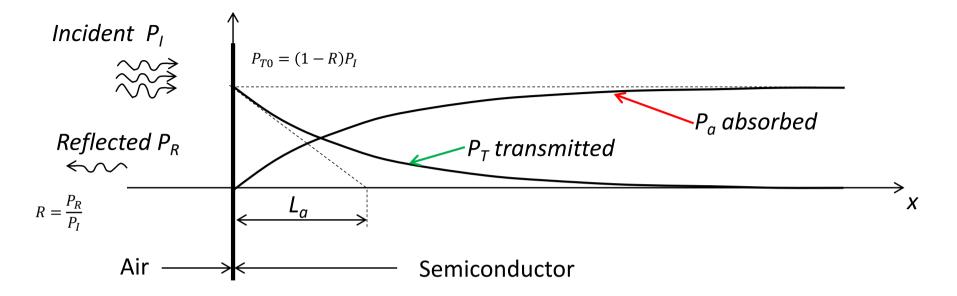


At the surface strong discontinuity of the refraction index *n*, from n = 1 for air to n > 1 for semiconductor: e.g. for silicon it is about  $n \approx 3,4$  and depends on the wavelength. This discontinuity gives a **high reflection coefficient** *R* 

 $R = \frac{P_R}{P_I}$  (e.g. for silicon R > 0,4 wavelength dependent )

**Anti-reflection coating**: deposition on the reflecting surface of a sequence of thin dielectric material layers with progressively decreasing *n* value. It provides a **gradual decrease** of the n value from semiconductor to air and such a smoother transition reduces the reflection

## **Absorption of Photons in materials**



For moderate or low  $P_T$  the absorption in dx is proportional to  $P_T$  (linear optic effect)

$$-dP_T = \alpha P_T dx = P_T \frac{dx}{L_a} \qquad \qquad \alpha = \text{optical}$$
$$L_a = 1/\alpha = 0$$

The optical power transmitted to position *x* is

$$P_T = P_{T0} \exp(-\alpha x) = P_{T0} \exp\left(-\frac{x}{L_a}\right)$$

The optical power absorbed from 0 to x is

$$P_a = P_{T0} - P_T = P_{T0}(1 - e^{-\alpha x}) = P_{T0}(1 - e^{-\frac{x}{L_a}})$$

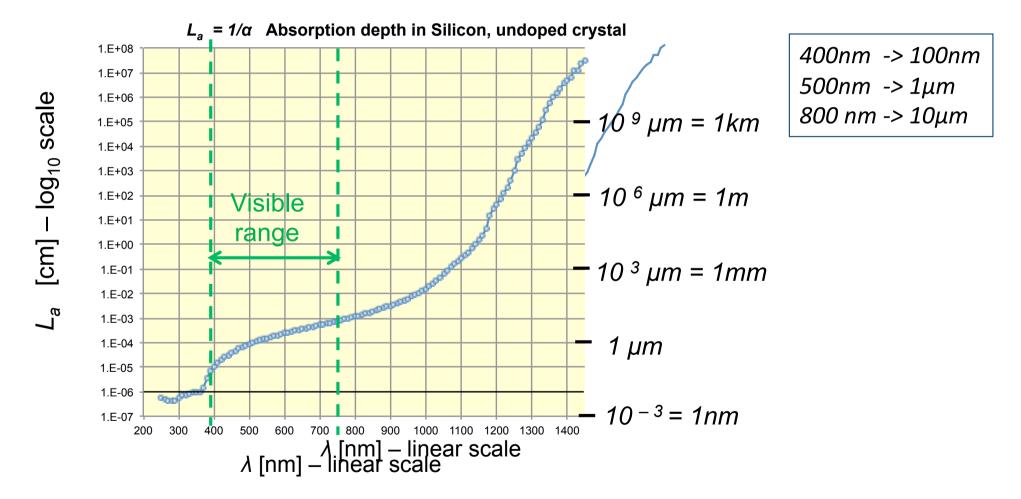
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 $\alpha$  = optical absorption coefficient  $L_{\alpha} = 1/\alpha$  = optical absorption depth

## **Absorption of Photons**

For a given material the optical absorption **STRONGLY** depends on the **WAVELENGTH**.

Typical example: Silicon absorption depth



NB: over the visible range  $L_a$  varies with  $\lambda$  by two orders of magnitude!!

# **Thermal Photodetector Principles**

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## **Principle of Thermal Photodetectors**

- A principle for detection of light signals is to employ their energy simply for heating a target and measure its temperature rise ΔT. Detectors relying on this principle are called «Thermal Photodetectors» or «Power Detectors»
- Main advantage: very **wide spectral range**. Since photons just have to be absorbed for contributing to the detection, the range can be extended far into the infrared.
- Main drawback: **sensitivity is inherently poor**, because a high number of absorbed photons is required for producing even small variations of temperature  $\Delta T$  in tiny target. For instance:  $\approx 10^{15}$  blue photons are required for heating by  $\Delta T=0,1$  K a water droplet of  $\approx 1$ mm diameter (*blue photons at*  $\lambda=475$ *nm have*  $V_p = 2,6$  eV; water has specific heat capacity  $c_T = 4186 [J/Kg\cdot K] = 2,6 \cdot 10^{22} [eV/Kg\cdot K]$  and the mass is 1mg)
- The dynamic response is inherently slow, because thermal transients are slow. Thermal detectors are mainly suitable for measurement of steady radiation.

## **Radiant Sensitivity or Spectral Responsivity**

- Thermal detectors transduce the optical power *P<sub>P</sub>* in an electrical output signal *V<sub>D</sub>* of the temperature sensor.
- The basic quantitative characterization of the performance of the detector is given by the **Radiant Sensitivity** (also called Spectral Responsivity) S<sub>D</sub>, defined as

electrical output voltage [in V]

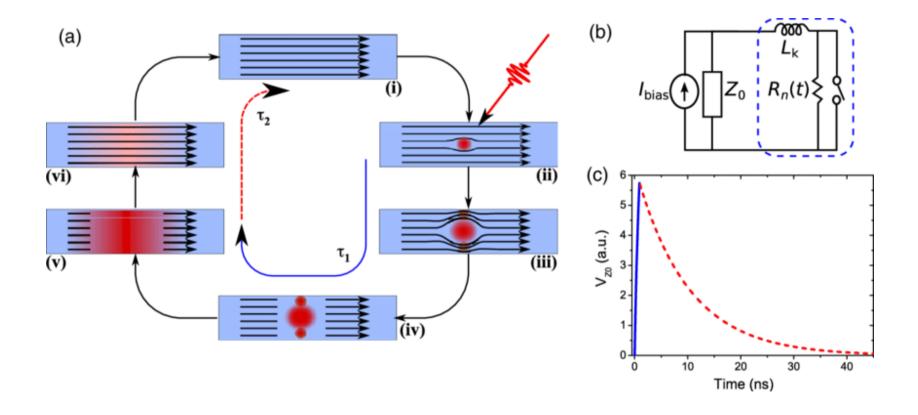
 $S_D =$ 

optical power on the detector sensitive area [in W]

 For a given absorbed power the detector is heated at a given level, independent of the radiation wavelength λ. Therefore, uniform S<sub>D</sub> would be obtained at all λ if the reflection and absorption were constant, independent of λ.

# **Superconducting nanowire**

## Superconducting nanowire single-photon detectors



Natarajan, Chandra & Tanner, Michael & Hadfield, Robert. (2012). Superconducting nanowire single-photon detectors: Physics and applications. Superconductor Science & Technology - SUPERCONDUCT SCI TECHNOL. 25. 10.1088/0953-2048/25/6/063001.

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# **Quantum Photodetector Principles**

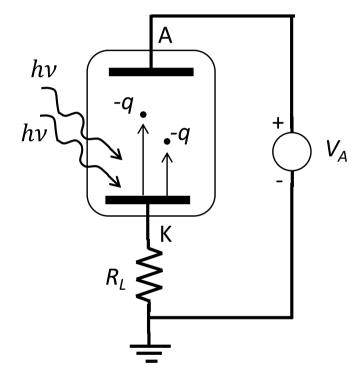
## **Principles of Quantum Photodetectors**

 A different principle for the detection of light signals is to exploit photo-electric effects for producing directly an electrical current in the detector. The energy of the absorbed photons is used for generating free charge carriers, which constitute the elements of the detector current.

 Detectors relying on this principle are called «Quantum Photodetectors» or «Photon Detectors»

• Photon Detectors can be vacuum-tube or semiconductor devices

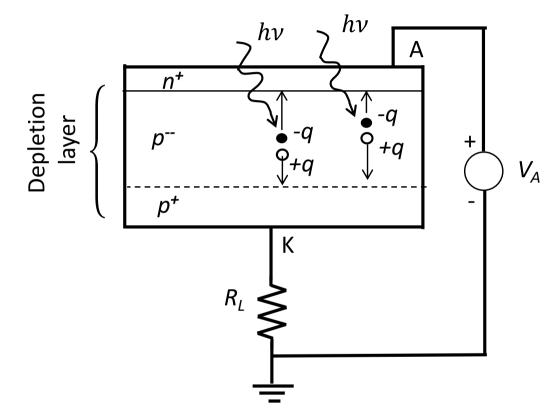
### **Principles of Quantum Photodetectors**



#### Vacuum-Tube detector devices: Photo-Tubes or Photo-Diodes

- An electrode (cathode K) in a vacuum enclosure receives the photons
- By **photo-electric effect** the cathode emits electrons in vacuum.
- The electrons are drawn by the electric field to another electrode biased at higher potential (anode A)
- Current flows through the terminals (photocathode and anode).

### **Principles of Quantum Photodetectors**



#### Semiconductor detector devices: Photo-Diodes

- Photons impact on a reverse-biased p-n junction diode
- The absorbed photons raise electrons from valence band to conduction band of the semiconductor, thereby generating free electron-hole pairs.
- The free carriers generated in the zone of high electric field (the depletion layer) are drawn by the junction electric field (the electrons to the n-terminal and the holes to the p-terminal)
- Current flows through the terminals.

## **Quantum Detection Efficiency**

- Quantum photodetectors transduce optical signals in electrical current signals by collecting the free electrons generated by the photons of the optical radiation.
- The basic quantitative characterization of the performance of the detector is given by the **Quantum Detection Efficiency** (or Photon Detection Efficiency)  $\eta_D$  defined as

number of photogenerated electrons (or electron-hole pairs)

number of photons reaching the detector

 However, since in many engineering tasks the focus is on the transduction from optical power to electrical current, the Radiant Sensitivity S<sub>D</sub> is often employed also for quantum photodetectors, defined as

electrical output current [in A]

*S*<sub>D</sub> = \_\_\_\_\_

$$=\frac{I_D}{P_L}\left[\frac{A}{W}\right]$$

optical power on the detector sensitive area [in W]

 $\frac{N_e}{N_p}$ 

## **Quantum Efficiency and Radiant Sensitivity**

Photons of wavelength  $\lambda$  arriving with steady rate  $n_p$  on a quantum detector convey an optical power  $P_L$ 

$$P_L = n_p h v$$

the electrons (or e-h pairs) photogenerated in the detector with steady rate  $n_e$ produce a current

$$I_D = n_e q$$

The Radiant Sensitivity is

$$S_D = \frac{I_D}{P_L} = \frac{n_e}{n_p} \cdot \frac{q}{h\nu} = \frac{n_e}{n_p} \cdot \frac{\lambda}{\frac{hc}{q}}$$

and since  $\eta_D = n_e/n_p$ 

$$S_D = \eta_D \cdot \frac{\lambda}{\frac{hc}{q}} = \eta_D \cdot \frac{\lambda[\mu m]}{1,24}$$



We see that the Radiant Sensitivity of the quantum detectors **intrinsically depends** on the wavelength  $\lambda$ , that is, even with constant quantum efficiency  $\eta_D$ . This occurs because a given optical power  $P_L$  corresponds to different photon rates  $n_p$  at different wavelengths  $\lambda$ 

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# **Photon Statistics and Noise**

## **Photon Noise**

- The optical radiation is composed of photons arriving randomly in time; the **photon number**  $N_p$  in a given time interval T is a statistical variable with mean  $\overline{N_p}$  and variance  $\sigma_p^2 = \overline{N_p^2} - (\overline{N_p})^2$
- The random fluctuations of the photons are the noise already present at optical level. This optical noise can be due to a background photon flux and to the actual desired optical signal.
- In most cases the photon statistics is well approximated by the Poisson statistics, so that it is

$$\sigma_p^2 = \overline{N_p}$$

• The optical power arriving to the detector is composed of quanta with energy hv arriving randomly at rate  $n_p$ . It is the analog at optical level of a shot electrical current: the mean optical power is  $P_p = n_p hv$  (analog to  $I_e = n_e q$ ); the shot optical noise has unilateral spectral density  $S_p$  (analog to  $S_i = 2qI_e$ )

$$S_p = 2h\nu P_p = 2\frac{hc}{\lambda}P_p$$

• Note that for a given optical power  $P_p$  the shot noise density decreases as the wavelength  $\lambda$  is increased

# Current Signals of Quantum Photodetectors

### **Detector Current Pulse Signal**

- In the transduction of optical signals to current signals by Quantum Photodetectors the dynamic response has a cut-off at high frequency. Ultrafast optical pulses are transduced to current pulses that are still fast, but have longer duration.
- The response to a multi-photon optical signal is the linear superposition of the elementary responses to individual photons. The response to a single photon is also called **Single-Electron-Response SER** because a photon generates just one free electron (or one electron-hole pair).
- It is simply wrong to consider the SER a δ-like current pulse occurring at the time where the photogenerated charge carrier impacts on the collector electrode. The carrier induces a charge in the collector electrode before reaching it; the induced charge varies with the carrier position, so that current flows during all the carrier travel in the electric field.
- The waveform of the current signal is obtained by taking the derivative of the charge induced on the collector electrode as a function of time. To compute this charge is an electrostatic problem not easy to solve in general. However, the mathematical treatment can be remarkably simplified by preliminarly computing the motion of the charge carriers and exploiting then the **Shockley-Ramo theorem**.

## **Shockley-Ramo theorem**

The output current due to an electron traveling towards the collector electrode can be obtained by applying the Shockley-Ramo theorem in three steps

- 1. The motion of the electron must be computed; i.e. the trajectory and the velocity  $v_c$  at every point of it must be known
- 2. A reference electric field  $E_v$  must be computed, which is the field that would exist in the device (in particular along the electron trajectory) under the following circumstances:

electron removed

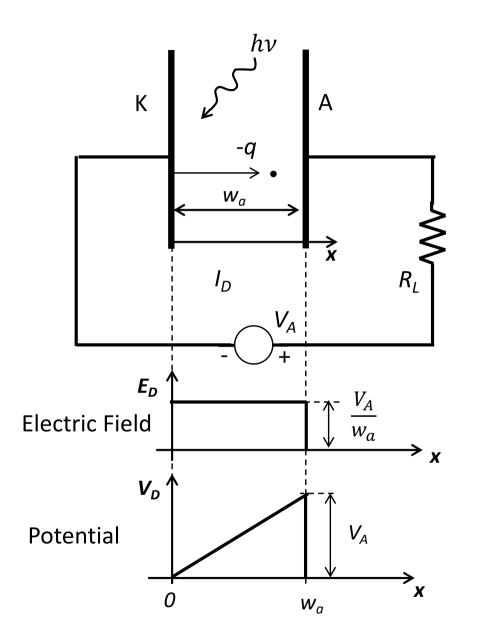
output electrode raised at unit potential

- all other conductors at ground potential
- 3. The **Shockley-Ramo theorem** states that the current  $i_c$  that flows at the output electrode due to the electron motion can be simply computed as

$$i_c = q \overrightarrow{E_v} \bullet \overrightarrow{v_c} = q E_{vc} v_c$$

where • denotes scalar product and  $E_{vc}$  is the component of the field  $\overrightarrow{E_v}$  in the direction of the velocity  $\overrightarrow{v_c}$ 

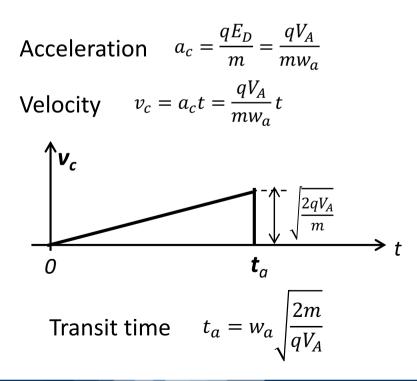
## **Carrier motion in a phototube (PT)**



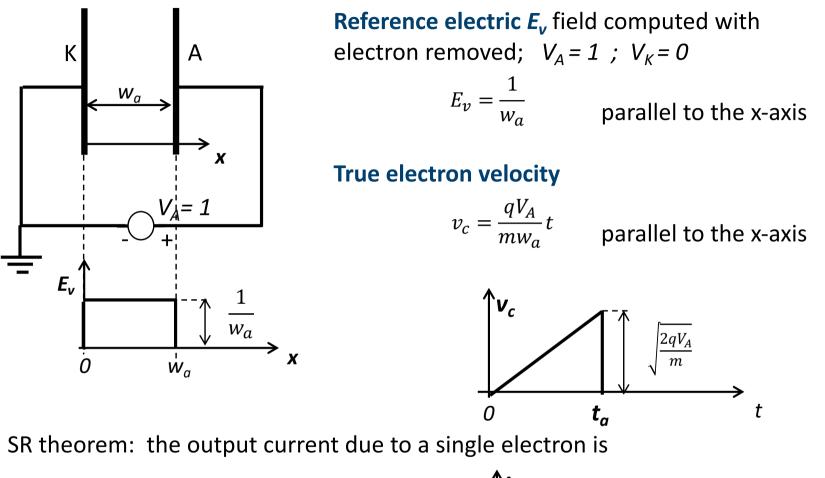
#### VACUUM PHOTOTUBE WITH PLANAR GEOMETRY

- $w_a$  = cathode to anode distance
- $V_A$  = bias voltage
- $E_D = \frac{V_A}{w_a}$  true electric field (in the x direction)
- $V_D = V_A \frac{x}{w_a}$  potential distribution

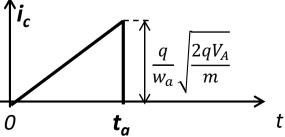
#### **ELECTRON MOTION IN VACUUM**



## **SER current in a phototube (PT)**



$$i_c = qE_v v_c = \frac{q^2 V_A}{m w_a^2} t$$



## **SER current in a phototube (PT)**

In a phototube with planar geometry the **single electron response (SER)** is a pulse with triangular waveform

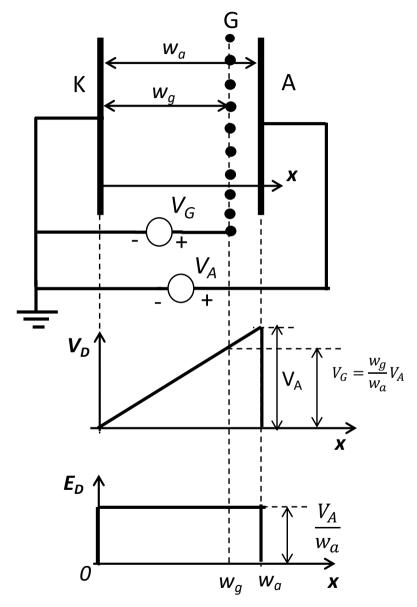
The frequency response is the Fourier transform of the SER pulse, which has a high frequency cutoff inversely proportional to the pulse width.

The pulse width is set by the transit time  $t_a$  of the electron from cathode to anode

$$t_a = \sqrt{2\frac{m}{q}} \cdot \frac{w_a}{\sqrt{V_A}} = 3,37 \cdot 10^{-6} \frac{w_a}{\sqrt{V_A}}$$

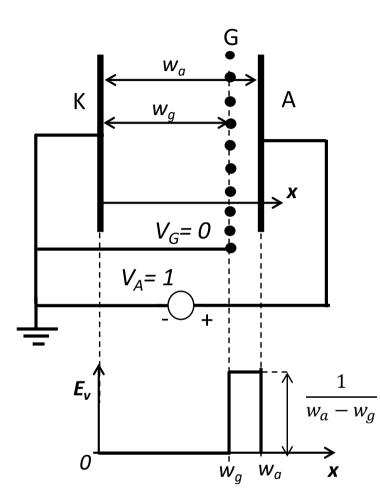
Typical values for phototubes are around w = 1cm = 0,01m and  $V_A = 100V$ , which correspond to transit time around  $t_a \approx 3,3$  ns

### **Screened-Anode PT: carrier motion**



- A shorter SER pulse can be obtained by inserting a metal wire grid in front of the anode
- The basic idea is that the grid acts as
   electrostatic screen that does not allow an
   electron traveling from x=0 (cathode) to x=w<sub>g</sub>
   (grid) to induce charge on the anode.
- The grid bias voltage is selected to minimize the perturbation to the electron motion; i.e. it is set to the potential V<sub>G</sub> corresponding to x=w<sub>g</sub> in absence of the grid (or slightly below it).
- In these conditions, the electric field is practically the same as in the phototube structure without grid and the motion of an electron in vacuum is also the same.

### **Screened-Anode PT: SR theorem**



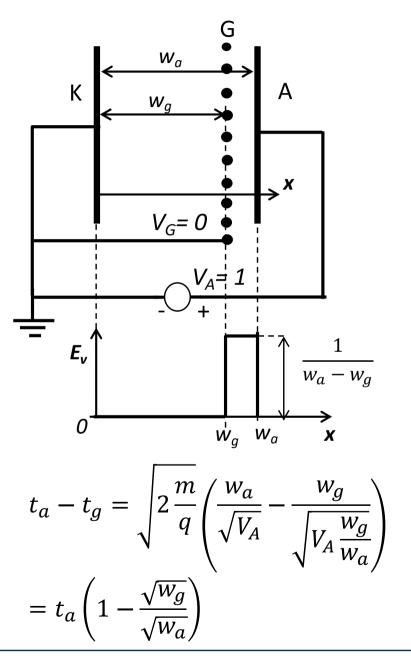
- Same electron motion as in the phototube without grid
- Different evolution in time of the induced charge on the anode.
- In fact, the reference field *E<sub>v</sub>* is now very different and neatly shows that charge is induced on the anode only during the last part of the electron trajectory, i.e. from *x*=*w<sub>q</sub>* (grid) to *x*=*w<sub>a</sub>* (anode)

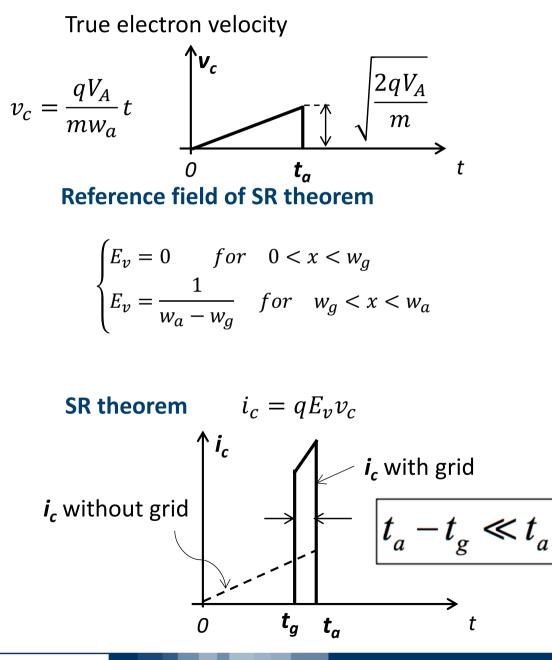
$$\begin{cases} E_v = 0 & for \quad 0 < x < w_g \\ E_v = \frac{1}{w_a - w_g} & for \quad w_g < x < w_a \end{cases}$$

• The SR theorem states that the SER current is

$$i_c = q E_v v_c$$

### **Screened-Anode PT for faster response**





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