

COURSE OUTLINE

- Introduction
- Signals and Noise
- **Filtering: High-Pass Filters 2 – HPF2**
- Sensors and associated electronics

- Measuring pulse signals in presence of $1/f$ noise with constant-parameter filters
- Basic constant-parameter High-Pass Filter (CR differentiator)
- Constant-Parameter High-Pass Filters in measurements of pulses in sequence
- Switched-Parameter High-Pass Filter: the Baseline Restorer

Measuring pulse signals in presence of $1/f$ noise

Case: amplitude measurement of **pulse** signals with **$1/f$** and **wideband** noise.

The **classic approach** to optimum filtering (to find first a noise-whitening filter and then a matched filter) **is arduous in this case because $1/f$ noise**

- sets a remarkably difficult mathematical problem
- makes the whitening filter difficult to design, not implementable with lumped circuit components, but with distributed parameters (distributed RC delay lines, etc.)

However, by noting that

a) for **$1/f$ noise** the filtered power

- mainly depends on the span of the band-pass measured by the **bandlimit ratio**, hence it is **markedly sensitive to the lower bandlimit level**
- **weakly** depends on the **shape** of the filter weighting function

b) for **wideband noise** the S/N

- depends on the span of the band-pass measured by the **bandlimit difference**, hence it is **weakly sensitive to the lower bandlimit level**
- markedly depends on the shape of the weighting function

an alternative approach leading to quasi-optimum filtering can be devised

FIRST STEP:

- Design a **main filter** for signal and wideband noise only (that is, considering non-existent the 1/f noise) and then
- Take then into account the 1/f component and evaluate the **additional noise power** that 1/f noise brings to the main filter output.

In the (lucky) cases where this 1/f noise power is smaller than the wide-band noise (or at least comparable), the main filter may be considered sufficient without further filtering.

Otherwise, if the addition due to 1/f noise is excessive, proceed to the

SECOND STEP :

- design an **additional filter** for limiting the 1/f noise power without worsening excessively the filtering of the wideband noise.

It is obviously a **high-pass filter**, which must combine the goal of

a) reducing efficiently the 1/f noise power

with the further requirements of

b) **limiting** to tolerable level the **increase of the filtered wide-band noise**

c) **limiting** to tolerable level the **reduction of the output signal amplitude**

The issue is better clarified by considering as FIRST STEP the **optimum filter for signal and wide-band noise (or its approximation)** composed by

- Noise-whitening filter, with output white noise S_B and pulse signal.
Let f_S be the upper band-limit and A the center-band amplitude of the pulse transform.
- Matched filter, which has weighting function matched to the pulse signal from the whitening filter and is therefore a low-pass filter with upper bandlimit f_S .
The output has a signal with amplitude roughly $V_S \approx A f_S$ and band-limited white noise with band-limit f_S and power

$$\overline{n_B^2} \approx S_B f_S$$

For focusing the ideas, let's consider a well known specific case: filtering of pulse-signals from a high impedance sensor with an approximately optimum filter, i.e. with matched filter approximated by a constant-parameter RC integrator.

In this case, the output noise corresponding to the input wide-band noise is a white noise spectrum with band-limit set by a pole with time constant $RC=T_{nc}$

Let's now take into account also a 1/f noise source, which brings at the whitening filter output a significant 1/f spectral density $S_B f_C / f$.

At high frequency, the 1/f component is limited by the upper bandlimit f_S of the matched filter.

At low frequency, the 1/f component can be limited by a lower band-limit f_i set by an additional constant-parameter filter. With $f_i \ll f_S$ the output power of the 1/f noise can be evaluated as

$$\overline{n_{fn}^2} \approx S_B f_C \ln \left(\frac{f_S}{f_i} \right)$$

However, the constant-parameter high-pass filter operates also on the signal: it attenuates the low frequency components and thus causes a loss in pulse amplitude, hence a loss in S/N. The reduced amplitude is roughly evaluated as

$$V_S \approx A(f_S - f_i) = A f_S \left(1 - \frac{f_i}{f_S} \right)$$

For limiting the signal loss, f_i/f_S must be limited; e.g. for keeping loss < 5% it must be

$$\frac{f_i}{f_S} \leq 0,05 \quad \text{that is} \quad \ln \left(\frac{f_S}{f_i} \right) \geq 3$$

For reducing the 1/f noise to the white noise level or lower

$$S_B f_C \ln \left(\frac{f_S}{f_i} \right) \leq S_B f_S$$

We need that

$$f_C \leq \frac{f_S}{\ln \left(\frac{f_S}{f_i} \right)}$$

and since for keeping the signal loss <5% it must be $\ln \left(\frac{f_S}{f_i} \right) \geq 3$
we need to have

$$f_C < \frac{f_S}{3}$$

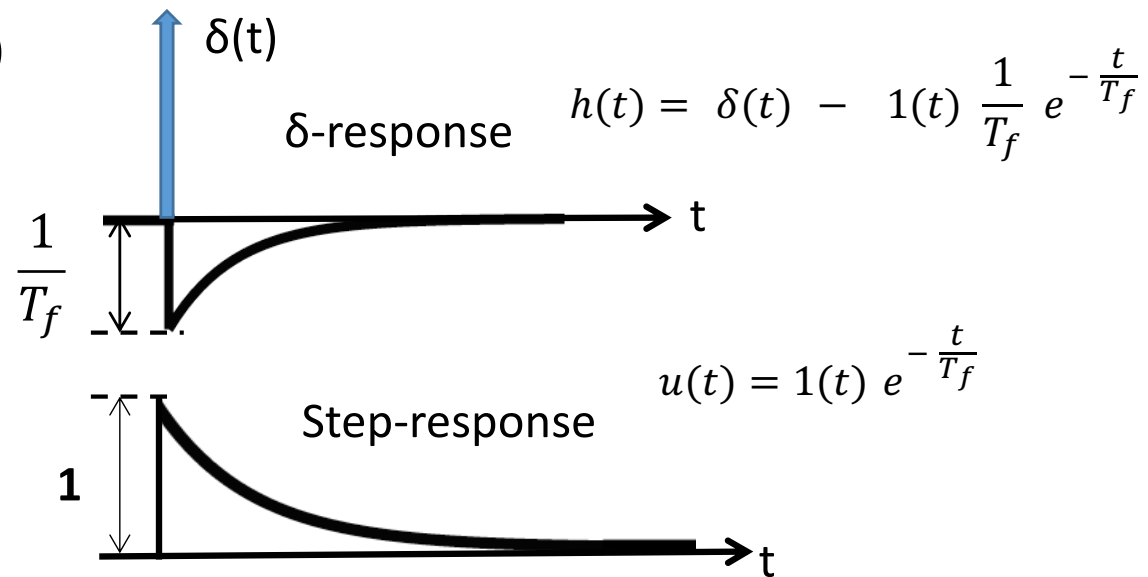
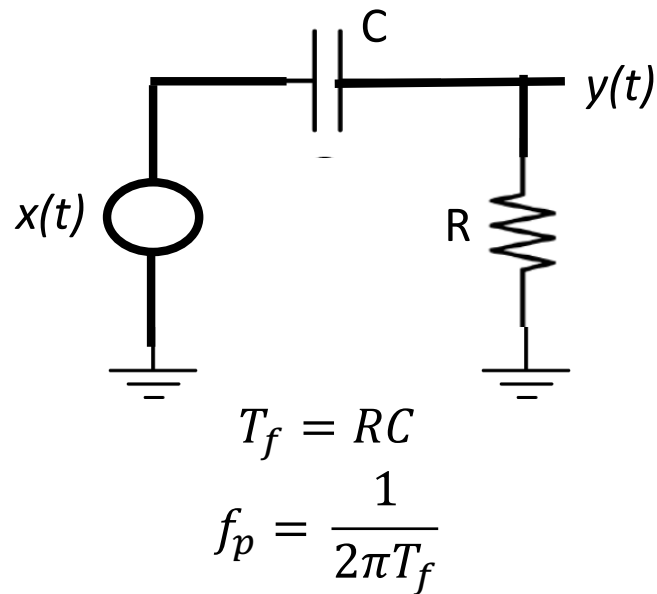
This means that the goal can be achieved only if the 1/f noise component is low or moderate. Note that **f_C and f_S are data** of the problem, they cannot be changed. In cases where f_C exceeds the above limit, a constant-parameter high-pass filter is NOT a suitable solution for reducing the 1/f noise power.

CONCLUSION: constant-parameter high-pass filters can be useful as additional filter for limiting the 1/f noise, but just in cases with moderate 1/f noise intensity, because of their detrimental effect on the signal pulse amplitude.

Basic constant-parameter High-Pass Filter (CR differentiator)

Basic High-Pass Filter (CR differentiator)

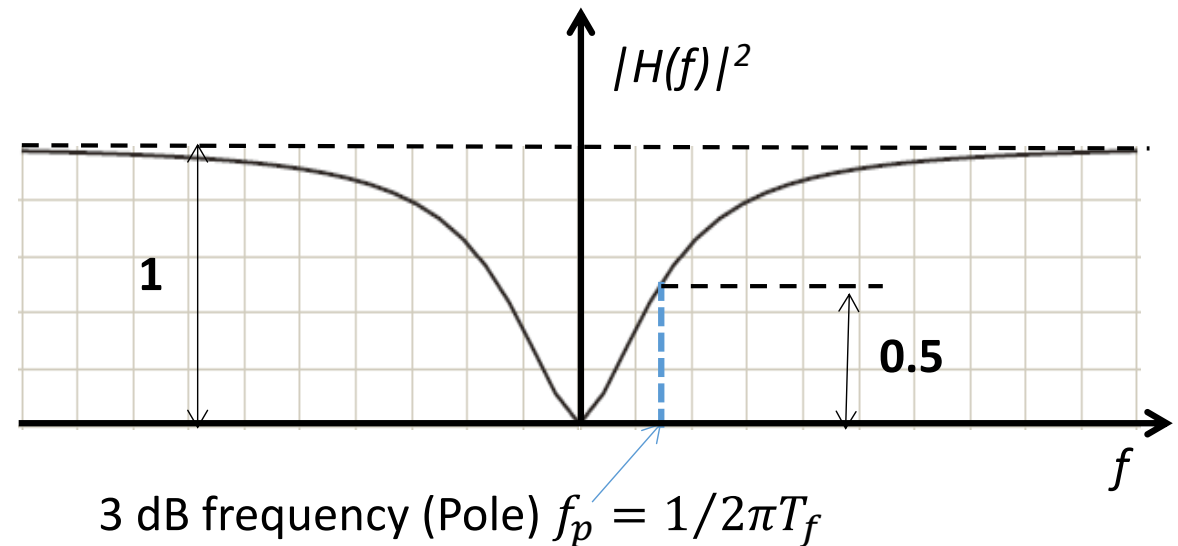
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Transfer function

$$H(f) = \frac{j 2\pi f T_f}{1 + j 2\pi f T_f}$$

$$|H(f)|^2 = \frac{(2\pi f T_f)^2}{1 + (2\pi f T_f)^2}$$



The intuitive view

«High-Pass Filter = All-Pass - Low-Pass Filter»

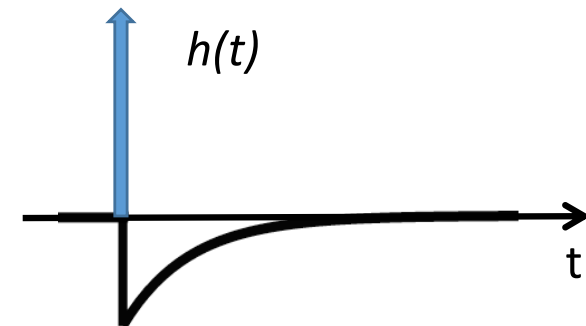
is confirmed by

Transfer function

$$H(f) = 1 - \frac{1}{1 + j 2\pi f T_f} = \frac{j 2\pi f T_f}{1 + j 2\pi f T_f}$$

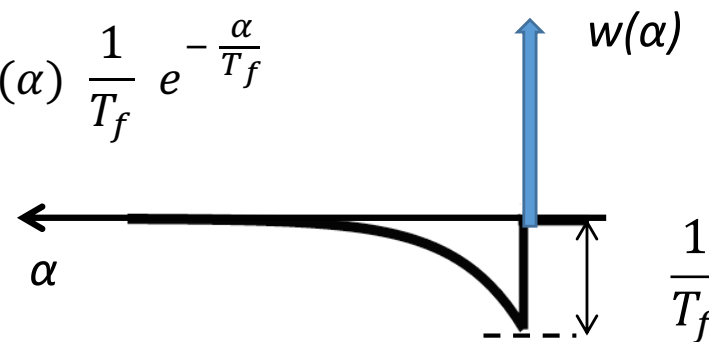
δ -response

$$h(t) = \delta(t) - 1(t) \frac{1}{T_f} e^{-\frac{t}{T_f}}$$



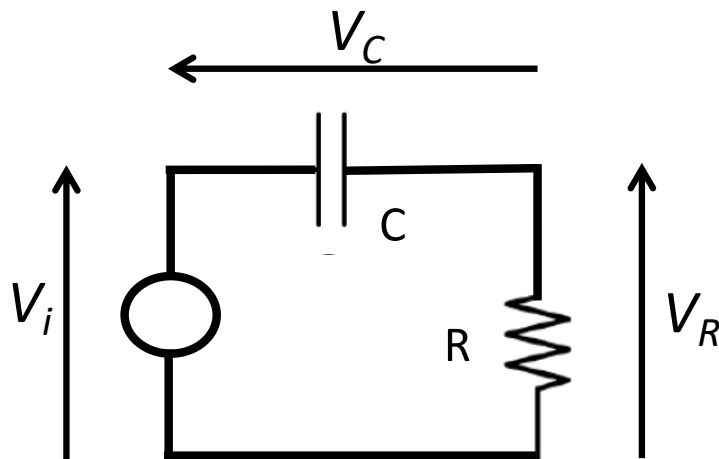
Weighting function

$$w(\alpha) = \delta(\alpha) - 1(\alpha) \frac{1}{T_f} e^{-\frac{\alpha}{T_f}}$$



The circuit mesh structure itself confirms that

«High-Pass Filter = All-Pass - Low-Pass Filter»



V_i = input voltage

V_C = low-pass filtered V_i

V_R = high-pass filtered V_i

Kirchoff's mesh voltage law

$$V_i = V_C + V_R$$

Therefore $V_R = V_i - V_C$
that is

High-pass filtered V_R = resistor voltage =
= input voltage V_i – capacitor voltage =
= input voltage V_i – Low-pass filtered V_i

High-pass band-limit for **White** noise

Premise: with only a high-pass CR filter the white noise power $\overline{n_B^2}$ is divergent, therefore we consider here also a low-pass filter with band-limit $f_s \gg 1/RC$.

The high-pass band-limit f_i of the CR filter with weighting function $W(f)$ is defined by

$$\overline{n_B^2} = S_B \int_0^{f_s} |W(f)|^2 df = S_B \int_0^{f_s} \frac{\left(\frac{f}{f_p}\right)^2}{1 + \left(\frac{f}{f_p}\right)^2} df = S_B(f_s - f_i)$$

The computation of the integral can be avoided by recalling that

CR high pass filter = all-pass – RC low-pass filter

and therefore

high-pass band-limit f_i of the CR filter = low-pass band-limit f_h of the RC filter

$$f_{iCR} = f_{hRC} = \frac{1}{4RC}$$

High-pass band-limit for $1/f$ noise

Premise: with only a high-pass CR filter the $1/f$ noise power $\overline{n_f^2}$ is divergent, therefore we consider here also a low-pass filter with a high band-limit $f_s \gg 1/RC$.

The high-pass band-limit f_{if} of the CR filter is defined by

$$\overline{n_f^2} = S_B f_c \int_0^{f_s} \frac{\left(\frac{f}{f_p}\right)^2}{1 + \left(\frac{f}{f_p}\right)^2} \frac{df}{f} = S_B f_c \int_{f_{if}}^{f_s} \frac{df}{f} = S_B f_c \ln\left(\frac{f_s}{f_{if}}\right)$$

In this case the first integral is fairly easily computed and shows that

$$f_{if} = \frac{f_p}{\sqrt{1 + \left(\frac{f_p}{f_s}\right)^2}}$$

that is, for $f_s \gg f_p$

$$f_{if} \approx f_p = \frac{1}{2\pi RC}$$

Band-limit of CR differentiator

$$\overline{n_f^2} = S_B f_c \int_0^{f_s} \frac{\left(\frac{f}{f_p}\right)^2}{1 + \left(\frac{f}{f_p}\right)^2} \frac{df}{f} = S_B f_c \frac{1}{2} \int \frac{g'(f)}{g(f)} df$$

Considering $g(f) = 1 + \left(\frac{f}{f_p}\right)^2$ and $g'(f) = 2 \frac{f}{f_p^2}$

We can solve the integral by substitution obtaining:

$$\overline{n_f^2} = S_B f_c \frac{1}{2} \ln \left(1 + \left(\frac{f_s}{f_p}\right)^2 \right)$$

And then make it equal to the final form:

$$\overline{n_f^2} = S_B f_c \frac{1}{2} \ln \left(1 + \left(\frac{f_s}{f_p}\right)^2 \right) = S_B f_c \ln \sqrt{\left(1 + \left(\frac{f_s}{f_p}\right)^2 \right)} = S_B f_c \ln \left(\frac{f_s}{f_{if}} \right)$$

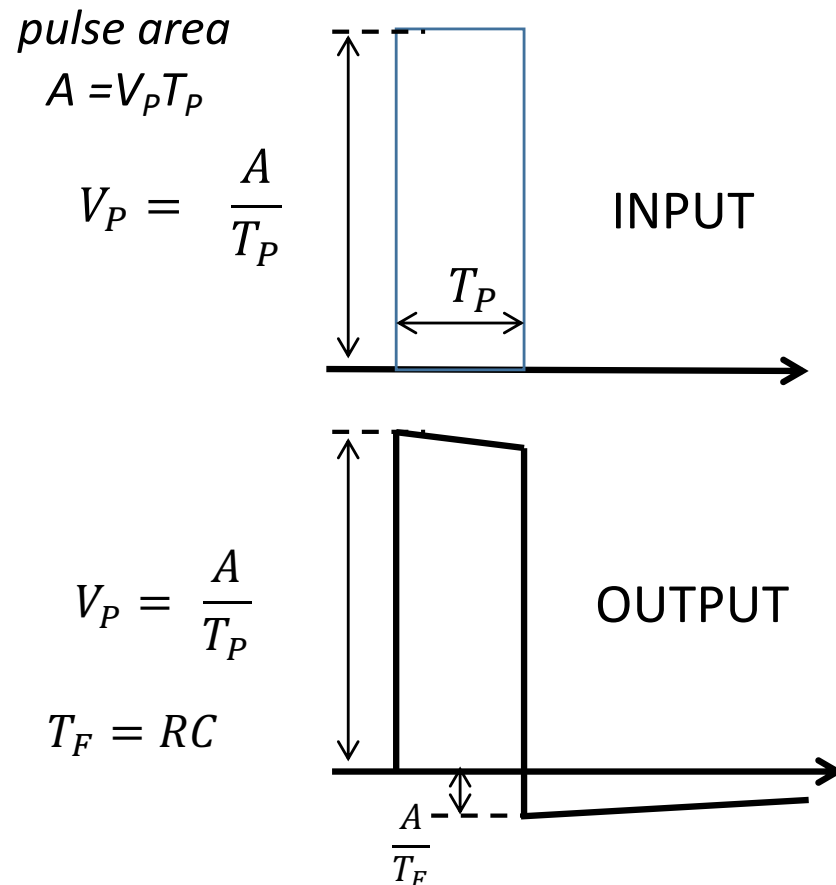
$$f_{if} = \frac{f_s}{\sqrt{1 + \left(\frac{f_s}{f_p}\right)^2}} = \frac{\frac{f_p}{f_s}}{\frac{f_p}{f_s} \sqrt{1 + \left(\frac{f_s}{f_p}\right)^2}} = \frac{f_p}{\sqrt{1 + \left(\frac{f_p}{f_s}\right)^2}}$$

- **The upper frequency limit f_s :**
 - is necessary for limiting the white noise power
 - is useful also for limiting the $1/f$ noise power
 - the level of f_s is dictated by the pulse signal to be measured
- **The lower frequency limit f_i :**
 - is necessary for limiting the $1/f$ noise power,
 - the selected level of f_i is conditioned by the pulse signal, it cannot be arbitrary
 - however, the reduction of $1/f$ noise is significant even with fairly low f_i , that is, with f_s/f_i values that are high, but anyway finite.

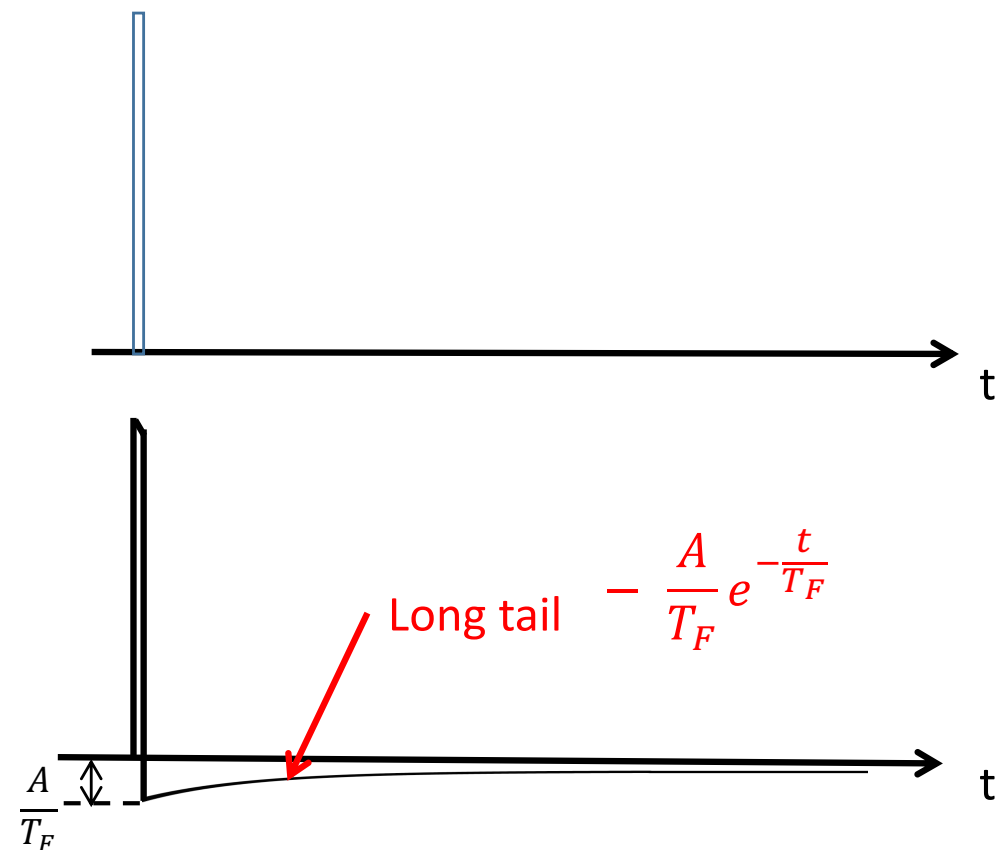
Constant-Parameter High-Pass Filters in measurements of pulses in sequence

Let's look in detail the effect of a high-pass filter ($RC = T_F$) on a pulse signal

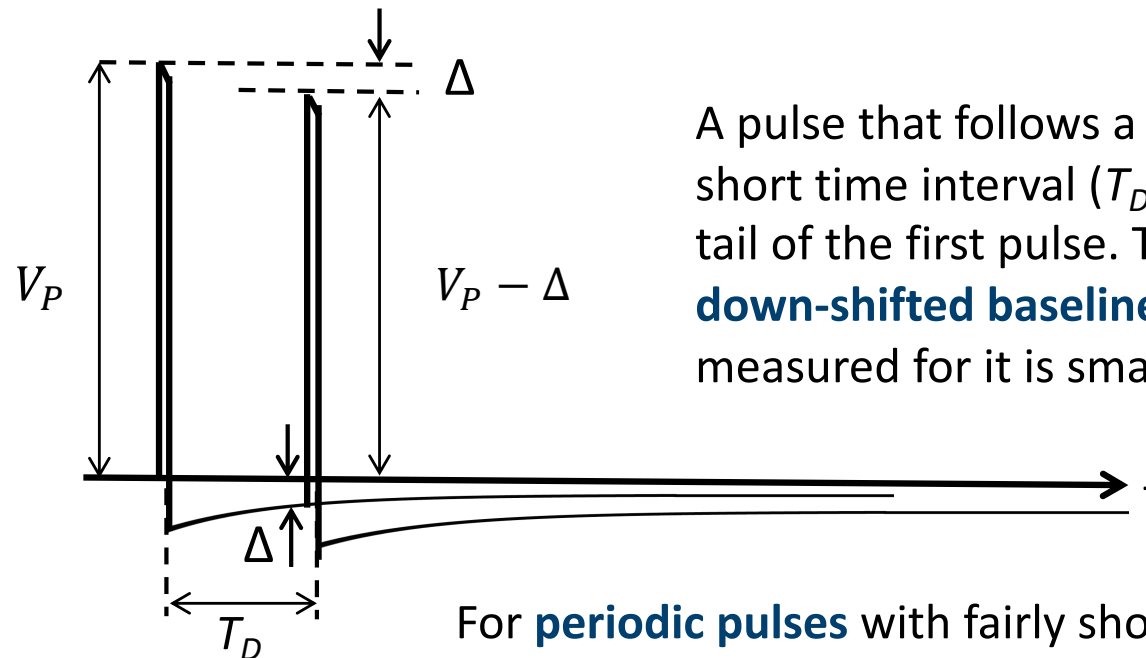
View on SHORT TIME scale



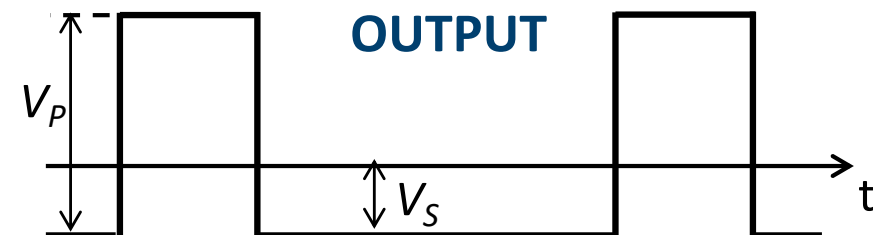
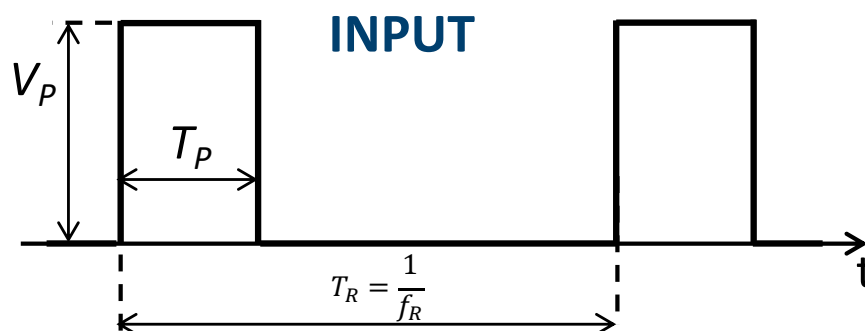
View on LONG TIME scale



NB: DC transfer of CR is zero \rightarrow net area of the output signal is zero



For **periodic pulses** with fairly short repetition period $T_R \ll T_F$, the superposition of slow pulse-tails shifts down the baseline by a V_S that makes zero the net area of the output signal



Repetition-rate-dependent baseline-shift

$$V_S = V_P \frac{T_P}{T_R} = A f_R$$

The high-pass filtering (differentiator action) of the CR filter has **MIXED effects**.

- The effect **on noise** is **ADVANTAGEOUS**: by cutting off the the low frequencies it markedly decreases the $1/f$ noise power (and mildly reduces the white noise power)
- The effect **on the signal** is **DISADVANTAGEOUS**:
 - it **decreases the signal amplitude** by cutting off the low frequencies of the signal , hence f_i must be kept low ($f_i \ll f_s$ of the pulse) in order to limit the signal loss. However, this limits also the reduction of $1/f$ noise
 - it **generates slow tails after the pulses**, which shift down the baseline and thus cause an error in the measured amplitude of a following pulse
 - With a **periodic** sequence of equal pulses, all pulses find the **same baseline shift**. The amplitude error is constant, sistematically dependent on the repetition rate.
 - With **random-repetition** pulses (e.g. pulses from ionizing radiation detectors) the pulses occur randomly in time. Hence the random superposition of tails produces a **randomly fluctuating baseline shift**. The resulting amplitude error is random: in this case the effect is equivalent to that of an additional noise source.

CONCLUSION: a differentiator action is **desirable on noise**, but **NOT on the signal**.

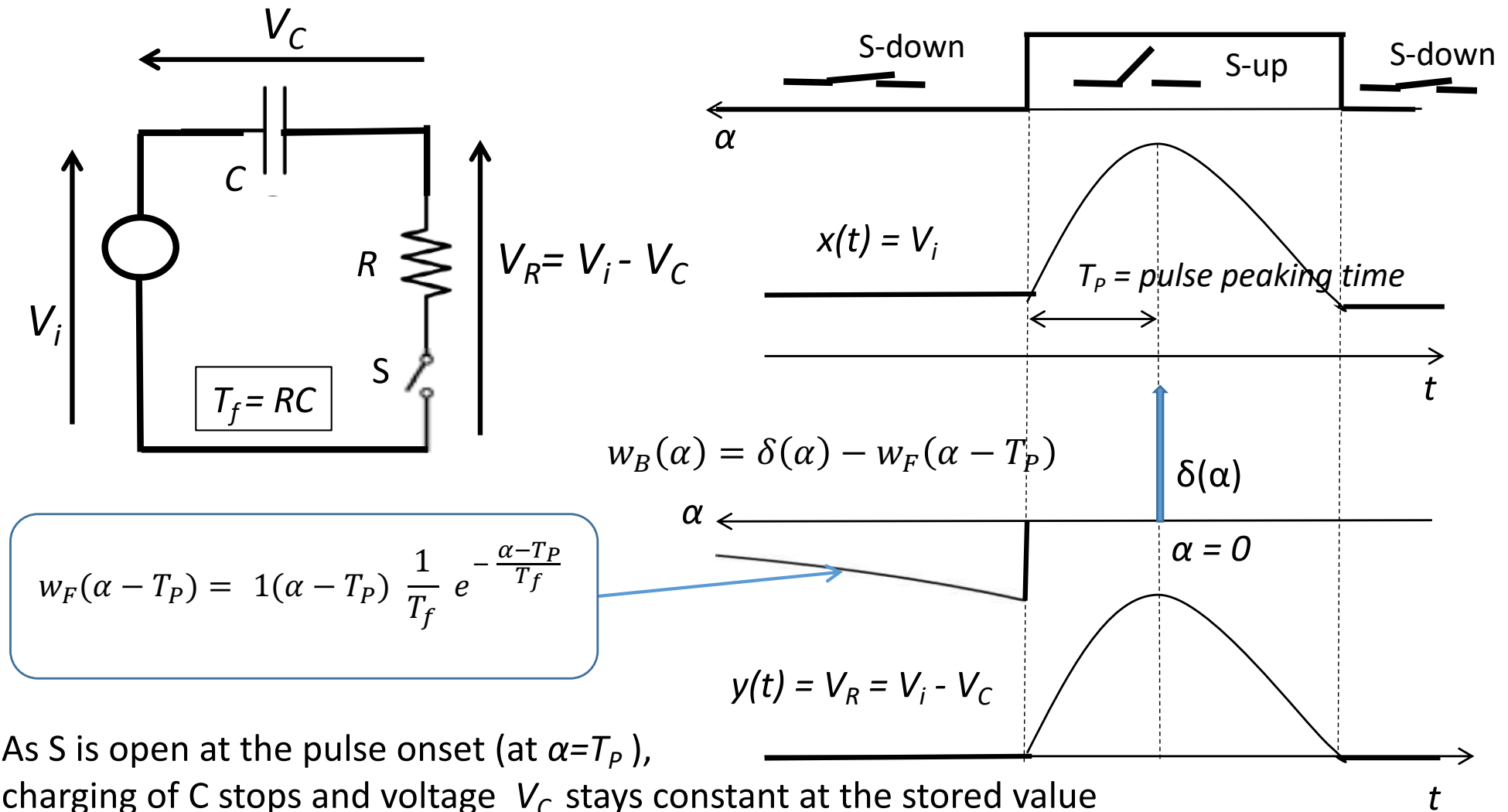
WANTED: not a constant-parameter differentiator, but a true **Base-Line Restorer (BLR)**

Switched-Parameter High-Pass Filter: the Baseline Restorer

Baseline Restorer (BLR) principle: switched CR

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High-pass filtering action **on the noise** and **NOT on the signal**: **switched-parameter** CR filter with $CR \rightarrow \infty$ when signal is present, finite $CR = T_f$ when no pulse is present

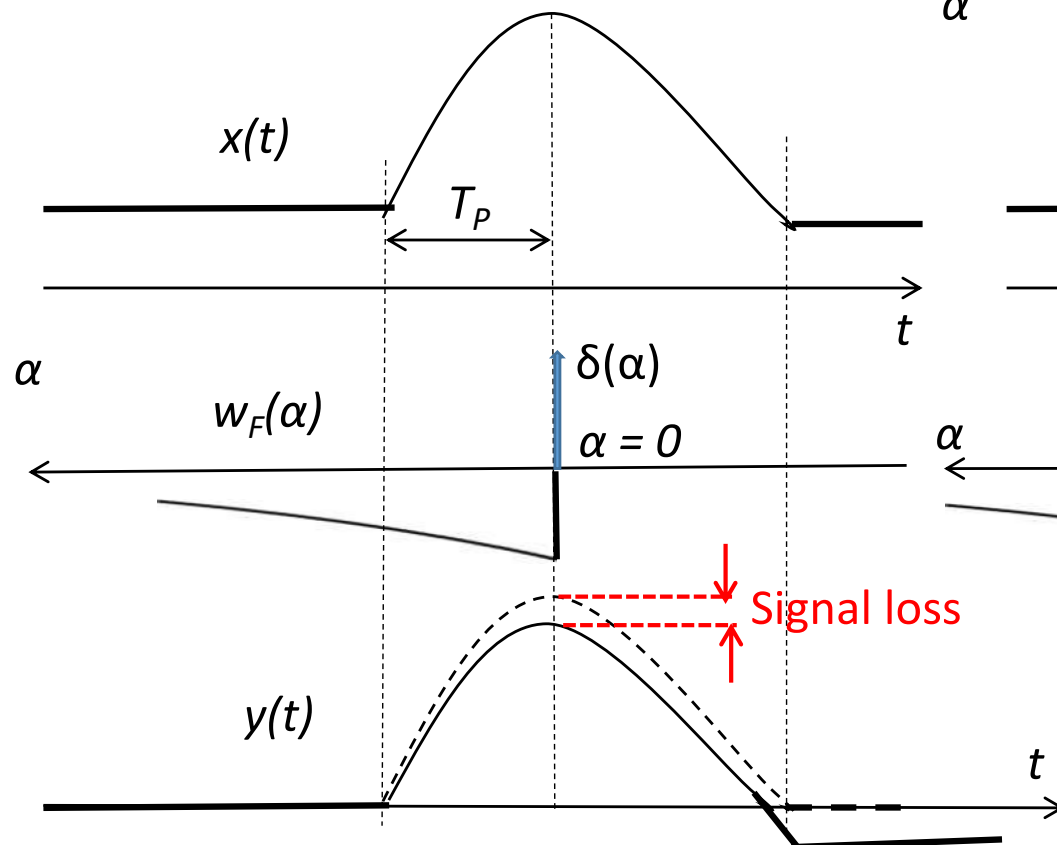


Comparing constant CR filter and BLR

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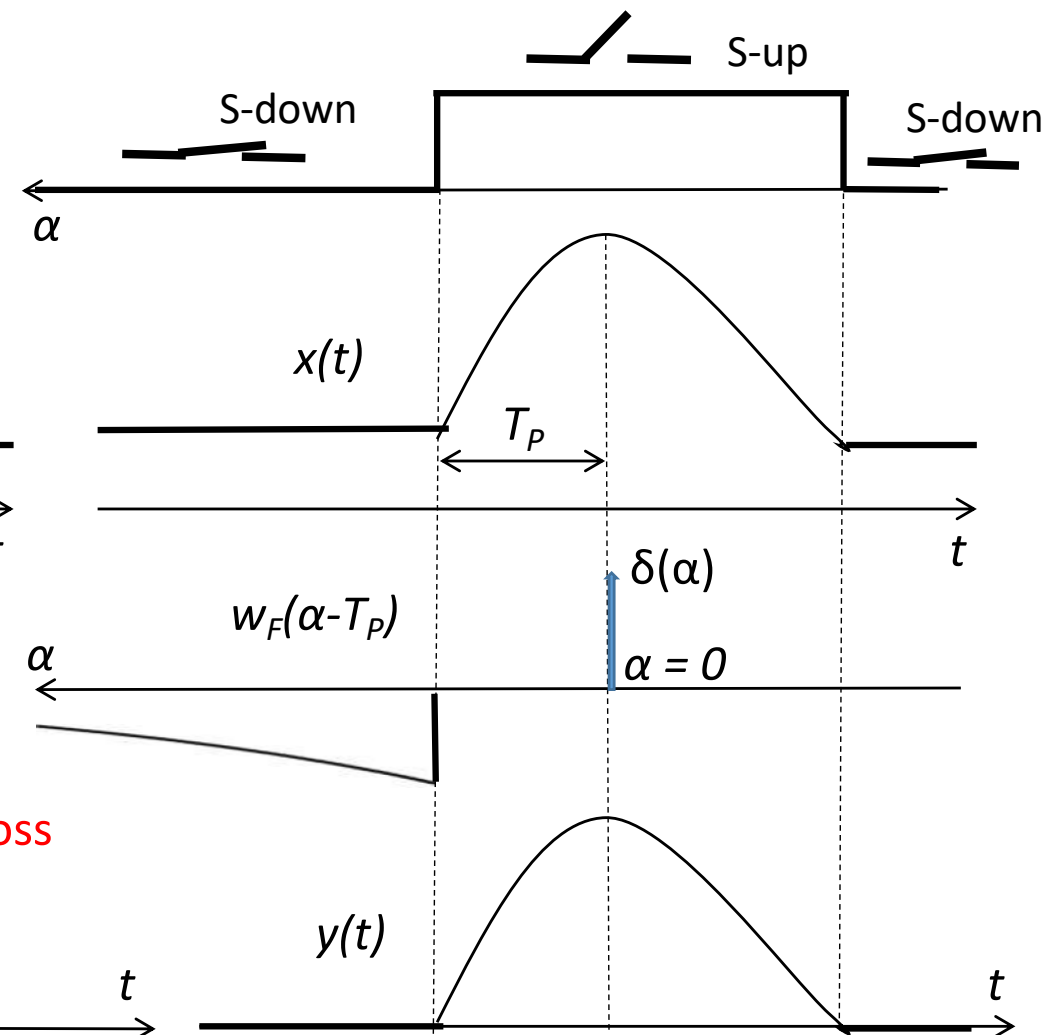
CONSTANT-PARAMETER FILTER

CR constant at all times

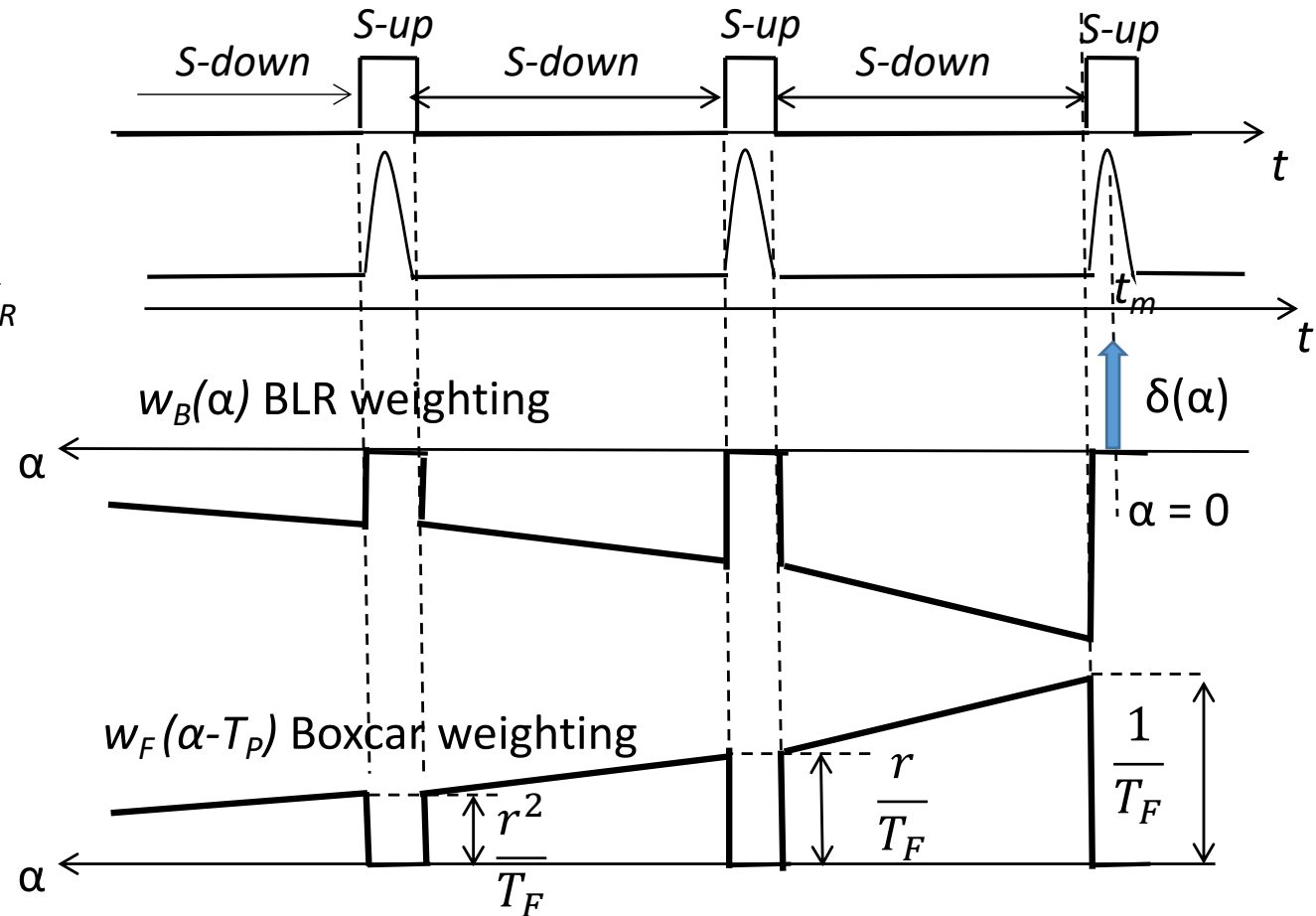
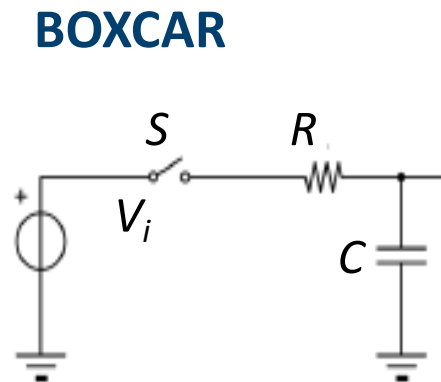
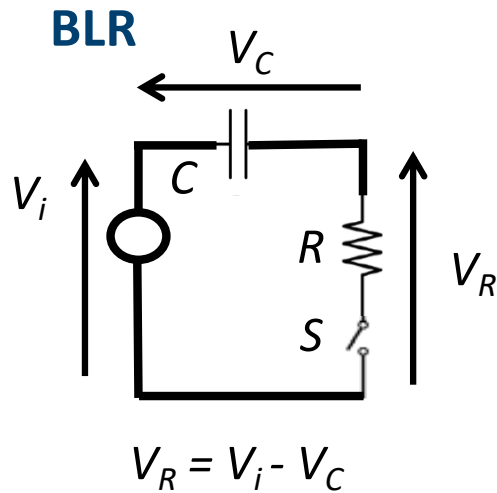


SWITCHED-PARAMETER FILTER

with S-up $R \rightarrow \infty$ and $CR \rightarrow \infty$

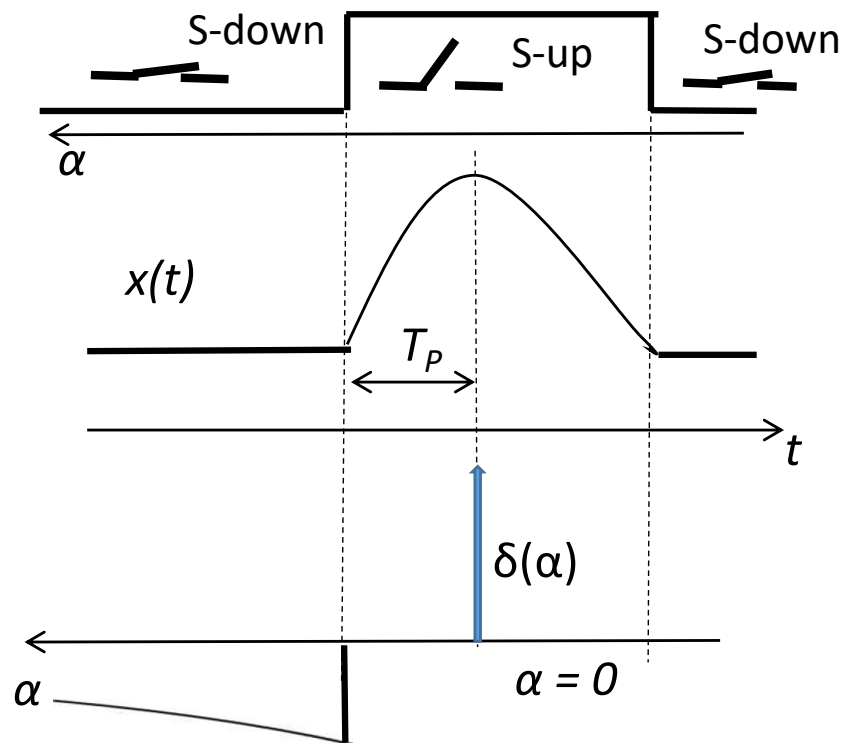


BLR = (All-Pass) – (Low-Pass Boxcar Integrator)



BLR weighting = (All-Pass – Low-pass Boxcar) weighting

$$w_B(\alpha) = \delta(\alpha) - w_F(\alpha - T_P)$$



BLR principle is alike filtered zero-setting,
but with a **basic advantage**:

much **shorter** T_P

much **higher band-limit** f_{if} (high-pass)

(the BLR switch is electronically controlled,
the interval T_P can be very short)

BLR weighting = All Pass – Low-pass

$$w_B(\alpha) = \delta(\alpha) - w_F(\alpha - T_P)$$

Low-pass weighting in frequency:

$$W_F(\omega) = F[w_F(\alpha)] = R_F(\omega) + i I_F(\omega)$$

BLR weighting in frequency:

$$\begin{aligned} W_B(\omega) &= 1 - e^{j\omega T_P} W_F(\omega) = 1 - [\cos \omega T_P - j \sin \omega T_P] \cdot [R_F + j I_F] = \\ &= [1 - R_F \cos \omega T_P - I_F \sin \omega T_P] - j [I_F \cos \omega T_P - R_F \sin \omega T_P] \end{aligned}$$

BLR weighting for noise:

$$\begin{aligned} |W_B(\omega)|^2 &= [1 - R_F \cos \omega T_P - I_F \sin \omega T_P]^2 + [I_F \cos \omega T_P - R_F \sin \omega T_P]^2 = \\ &= 1 + R_F^2 + I_F^2 - 2R_F \cos \omega T_P - 2I_F \sin \omega T_P = \\ &= 1 + |W_F|^2 - 2R_F \cos \omega T_P - 2I_F \sin \omega T_P \end{aligned}$$

Let's consider just cases where the interval between pulses is much longer than T_F so that

$$w_F(\alpha) = 1(\alpha) \frac{1}{T_f} e^{-\frac{\alpha}{T_f}} \quad \text{and} \quad W_F(\omega) = \frac{1}{1 + j\omega T_F}$$

and therefore

$$|W_B(\omega)|^2 = 1 + \frac{1}{1 + \omega^2 T_F^2} - 2 \frac{1}{1 + \omega^2 T_F^2} \cos \omega T_P + 2\omega T_F \cdot \frac{1}{1 + \omega^2 T_F^2} \sin \omega T_P$$

In the low-frequency region $\omega \ll \frac{1}{T_P}$ with the approximations

$$\sin \omega T_P \approx \omega T_P \quad \cos \omega T_P = 1 - \frac{\omega^2 T_P^2}{2}$$

we get

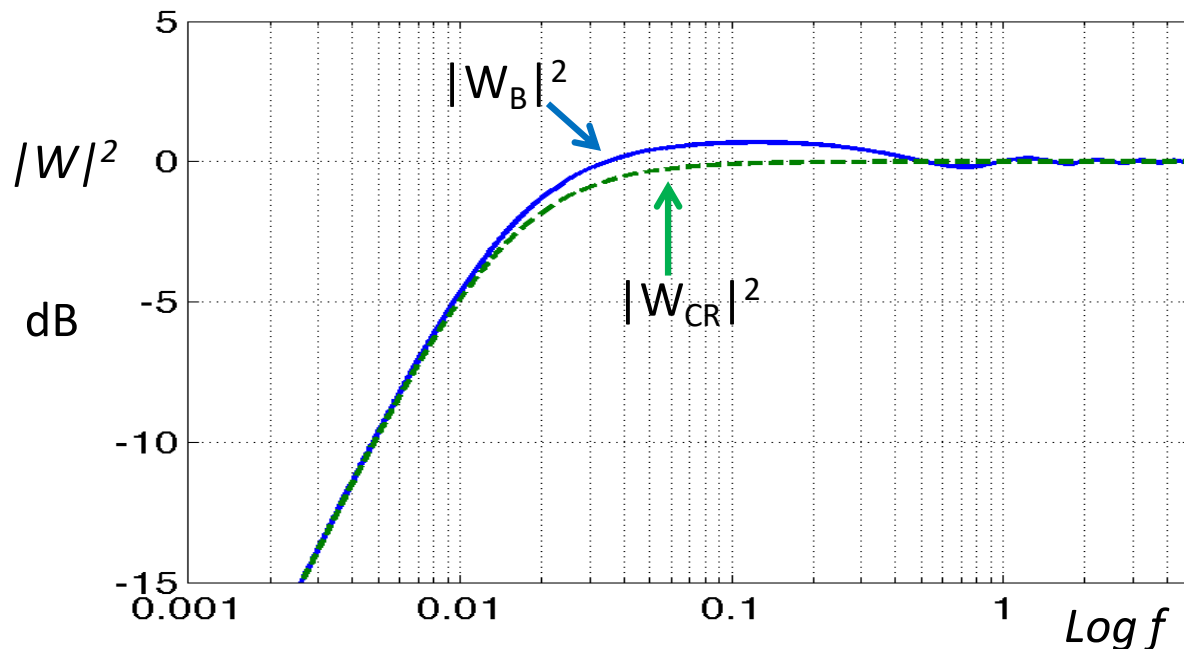
$$\begin{aligned} |W_B(\omega)|^2 &\approx 1 + \frac{1}{1 + \omega^2 T_F^2} - \frac{2}{1 + \omega^2 T_F^2} + \frac{\omega^2 T_P^2}{1 + \omega^2 T_F^2} + 2 \frac{\omega^2 T_P T_F}{1 + \omega^2 T_F^2} = \\ &= \frac{\omega^2 (T_P + T_F)^2}{1 + \omega^2 T_F^2} = \frac{\omega^2 T_F^2}{1 + \omega^2 T_F^2} \left(1 + \frac{T_P}{T_F}\right)^2 \end{aligned}$$

and in the lower region $\omega \ll \frac{1}{T_F} \ll \frac{1}{T_P}$

$$|W_B(\omega)|^2 \approx \omega^2 (T_P + T_F)^2$$

That is, the BLR has a cutoff equivalent to a CR high-pass with $RC = T_P + T_F$

BLR vs. CR High-Pass Filter: Cut-Off



BODE DIAGRAM
highlights
the low-freq cutoff

Example:
BLR with $T_P = 1$ and $T_F = 10$
CR filter with $RC = T_P + T_F$

$f \ll 1/T_F$
(i.e. $f \ll 0,1$ in the example)

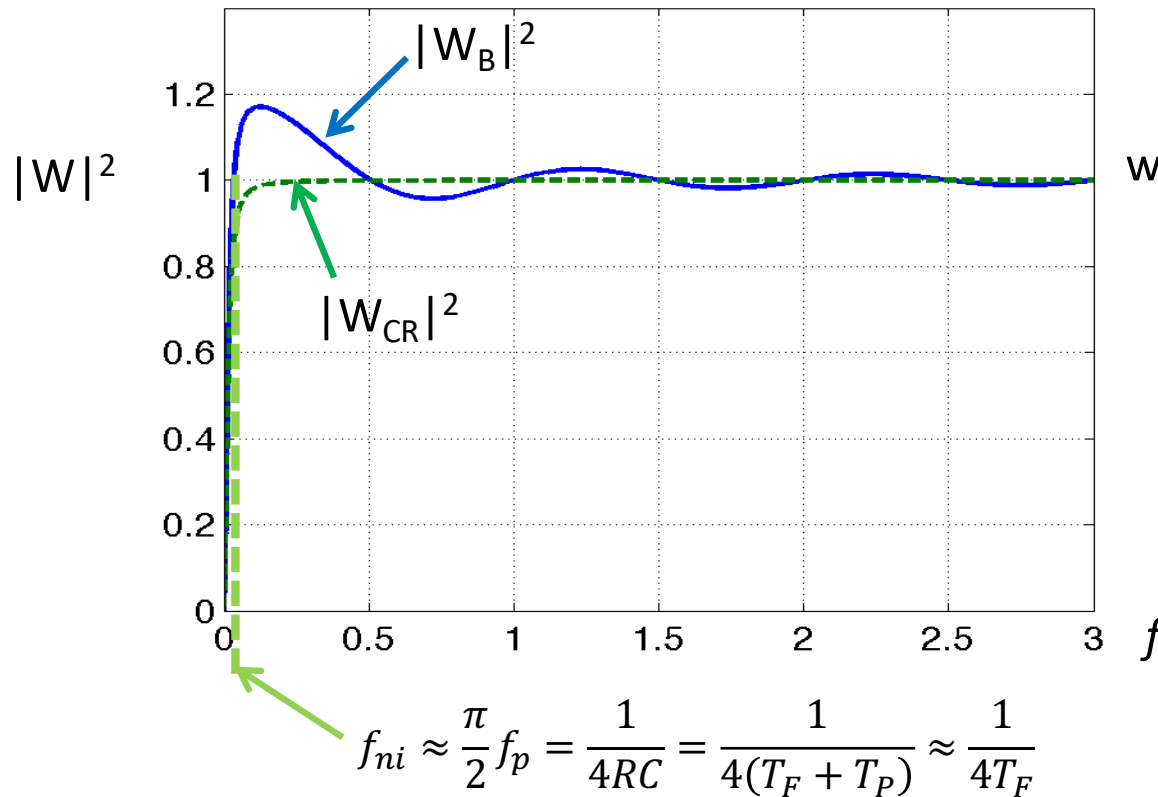
$$|W_B(\omega)|^2 \approx \omega^2 (T_P + T_F)^2$$

$$|W_{CR}(\omega)|^2 \approx \omega^2 R^2 C^2$$

$1/T_F < f \ll 1/T_P$
(i.e. $f \ll 1$ in the example)

$$|W_B(\omega)|^2 \approx \frac{\omega^2 (T_P + T_F)^2}{1 + \omega^2 T_F^2}$$

$$|W_{CR}(\omega)|^2 = \frac{\omega^2 R^2 C^2}{1 + \omega^2 R^2 C^2}$$

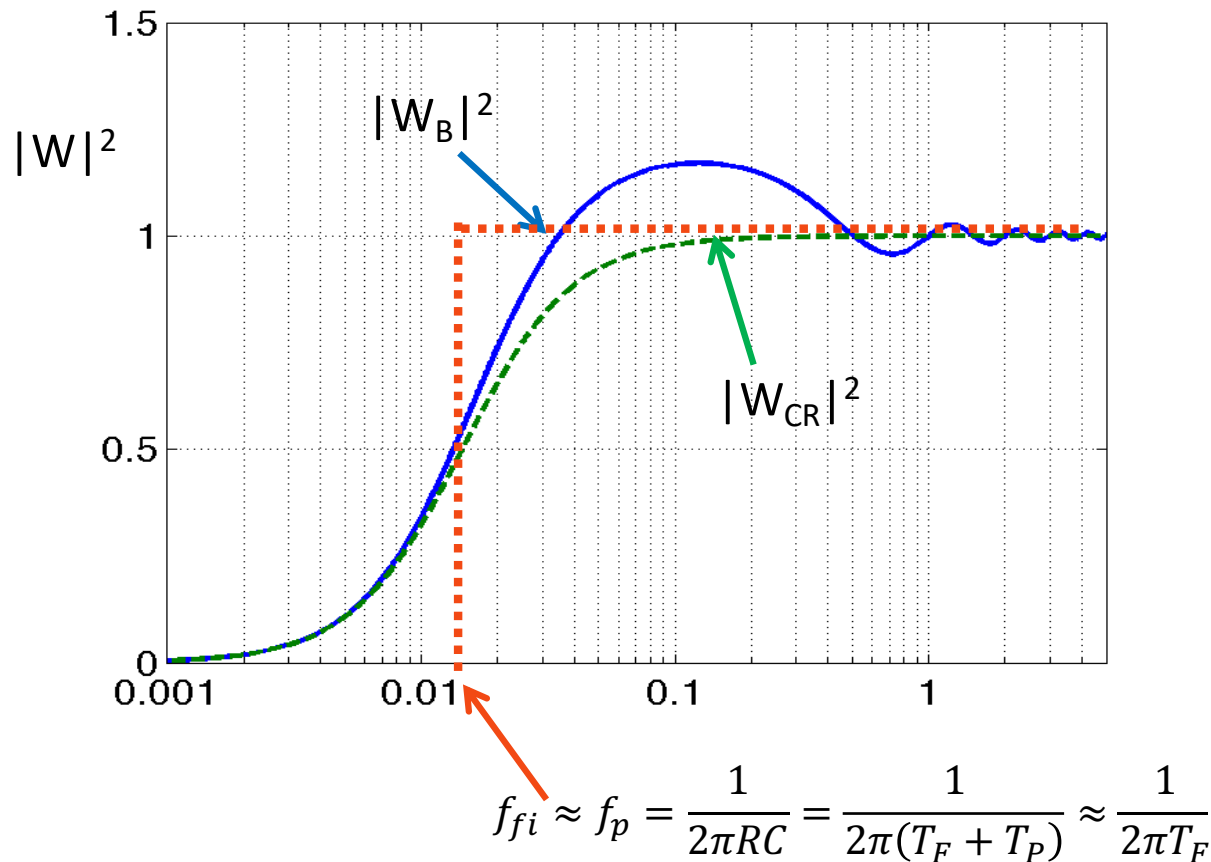


LIN –LIN DIAGRAM
 highlights
 white noise power \propto area of $|W|^2$

Example:
 BLR with $T_P = 1$ and $T_F = 10$
 CR filter with $RC = T_P + T_F$

f_{ni} = BLR high-pass band-limit for white noise. Note that:

- f_{ni} is equal to that of the equivalent CR High-pass filter
- f_{ni} is equal to bandlimit of the low-pass section in the BLR circuit



LIN –LOG DIAGRAM
highlights
 $1/f$ noise power \propto area of $|W|^2$

Example:
BLR with $T_P = 1$ and $T_F = 10$
CR filter with $RC = T_P + T_F$

f_{fi} = BLR high-pass band-limit for $1/f$ noise. Note that:

- f_{fi} is equal to that of the equivalent CR High-pass filter
- f_{fi} is equal to bandlimit of the low-pass section in the BLR circuit

The BLR filtering is ruled by:

1. **T_p time delay** from switch opening to pulse-amplitude measurement.

There is **no choice**: T_p is equal to the rise time from pulse onset to peak.

In fact, T_p can't be shorter than the rise of the pulse signal and should be as short as possible for filtering effectively of the $1/f$ noise.

2. **$T_F = RC$ differentiation time constant: to be selected** for optimizing the overall filtering of noise. The question is: how should T_F be selected for

- a) providing a good reduction of the $1/f$ noise power and
- b) avoiding to enhance significantly the white noise power

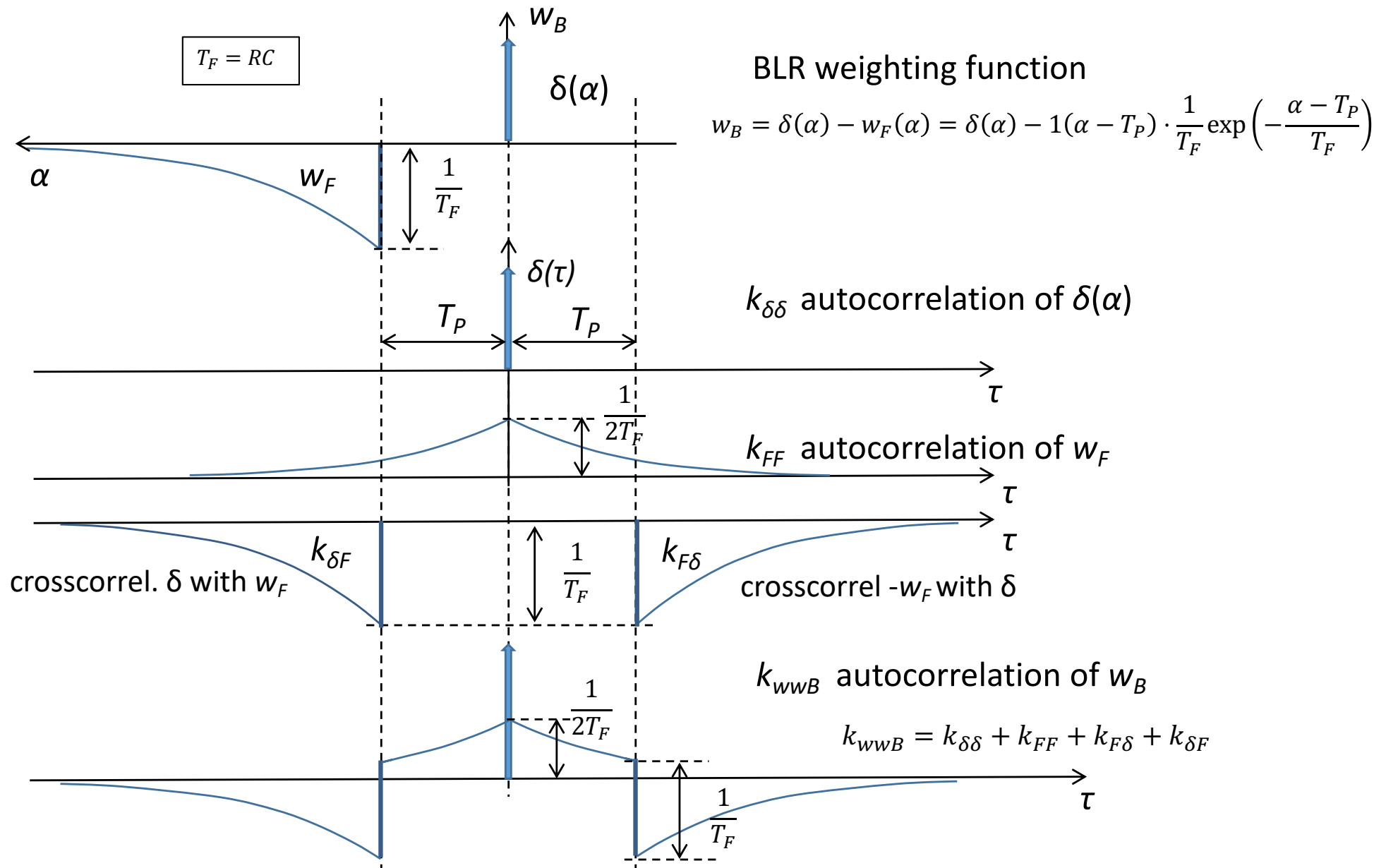
Since the BLR cutoff is set by $1/(T_p + T_F)$, a very short T_F might look advisable, but it is not: a BLR with $T_F \ll T_p$ operates like a CDS, hence it doubles the white noise and remarkably enhances also the $1/f$ noise above the cutoff frequency.

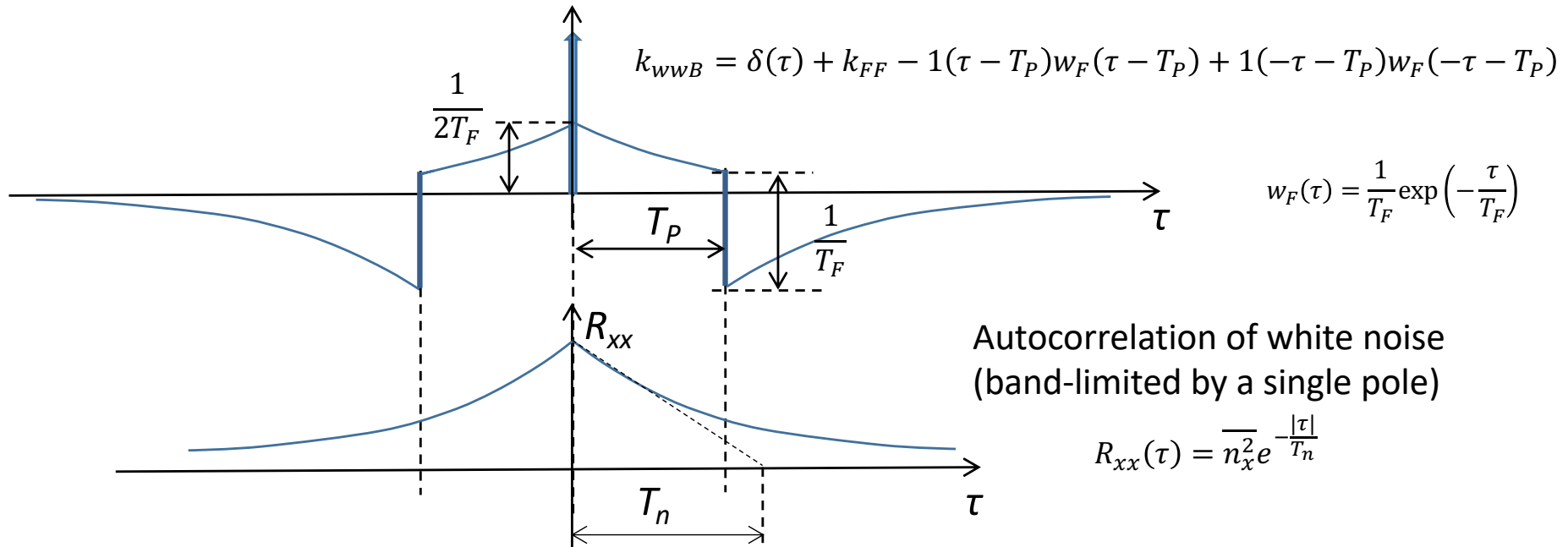
In the following discussion about the T_F selection, for focusing the ideas we will refer to a specific case: signals from a high impedance sensor processed by an approximately optimum filter, namely a CR-RC filter. The output corresponding to the input wide-band noise is a white spectrum band-limited by a simple pole. Such a situation is met in practice also in many other cases.

A better insight in the issue is gained with a **time-domain analysis of BLR filtering**

BLR Filtering of Noise: time-domain analysis

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$$\begin{aligned}
 \overline{n_B^2} &= \int_{-\infty}^{\infty} R_{xx}(\tau) k_{wwB}(\tau) d\tau = R_{xx}(0) + 2 \int_0^{\infty} R_{xx}(\tau) \frac{1}{2} w_F(\tau) d\tau - 2 \int_T^{\infty} R_{xx}(\tau) w_F(\tau - T_P) d\tau = \\
 &= R_{xx}(0) + \int_{-\infty}^{\infty} R_{xx}(\tau) \frac{1}{2} w_F(|\tau|) d\tau - 2 \int_0^{\infty} R_{xx}(\beta + T_P) w_F(\beta) d\beta
 \end{aligned}$$

Denoting

$$r_{xx}(\tau) = \frac{R_{xx}(\tau)}{R_{xx}(0)} = \frac{R_{xx}(\tau)}{\overline{n_x^2}}$$

We have

$$\overline{n_B^2} = \overline{n_x^2} \left\{ 1 + \int_{-\infty}^{\infty} r_{xx}(\tau) \frac{1}{2T_F} e^{-\frac{|\tau|}{T_F}} d\tau - 2 \int_0^{\infty} r_{xx}(\beta + T_P) \frac{1}{T_F} e^{-\frac{\beta}{T_F}} d\beta \right\}$$

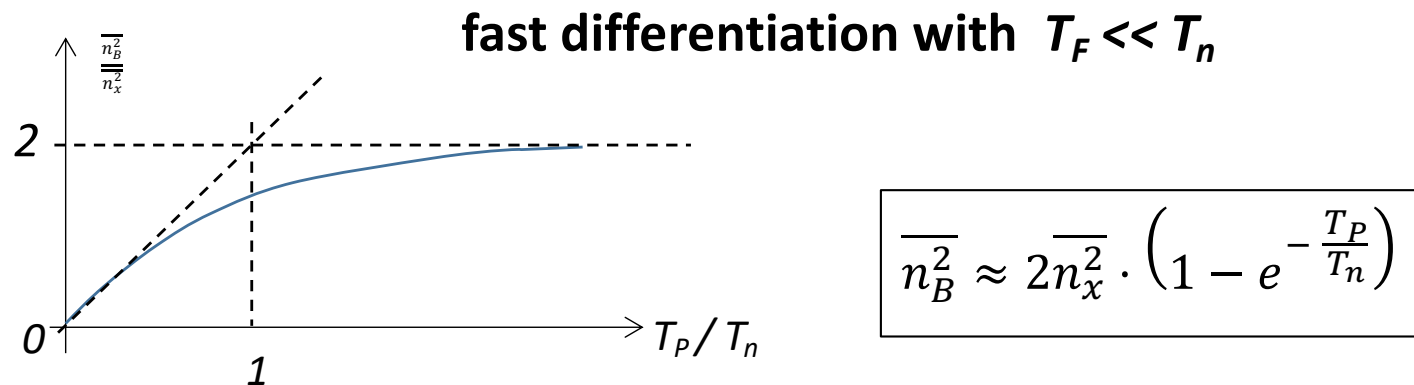
$$\begin{aligned}\overline{n_B^2} &= \overline{n_x^2} \left\{ 1 + \int_{-\infty}^{\infty} r_{xx}(\tau) \cdot \frac{1}{2T_F} e^{-\frac{|\tau|}{T_F}} d\tau - 2 \int_0^{\infty} r_{xx}(\beta + T_P) \cdot \frac{1}{T_F} e^{-\frac{\beta}{T_F}} d\beta \right\} \\ &= \\ &= \overline{n_x^2} \left\{ 1 + \frac{1}{2T_F} \int_{-\infty}^{\infty} e^{-|\tau|} \left(\frac{1}{T_F} + \frac{1}{T_n} \right) d\tau - 2e^{-\frac{T_P}{T_n}} \frac{1}{T_F} \int_0^{\infty} e^{-\beta} \left(\frac{1}{T_F} + \frac{1}{T_n} \right) d\beta \right\} = \\ &= \overline{n_x^2} \left[1 + \frac{T_n}{T_n + T_F} - 2e^{-\frac{T_P}{T_n}} \frac{T_n}{T_n + T_F} \right]\end{aligned}$$

and finally

$$\overline{n_B^2} = \overline{n_x^2} \left[1 + \frac{T_n}{T_n + T_F} \left(1 - 2e^{-\frac{T_P}{T_n}} \right) \right]$$

With **fast differentiation**, i.e. with $T_F \ll T_n$, it is quantitatively confirmed that the BLR acts like a CDS with $T=T_P$

$$\overline{n_B^2} \approx 2\overline{n_x^2} \cdot \left(1 - e^{-\frac{T_P}{T_n}} \right)$$



With $T_F \ll T_n$ the effect of BLR on **band-limited white noise** depends on how long is the correlation time T_n with respect to the delay T_P

- with **short correlation time** (wide band) the noise is **doubled**:

with $T_n < \frac{T_P}{5}$ it is $\overline{n_B^2} \approx 2\overline{n_x^2}$

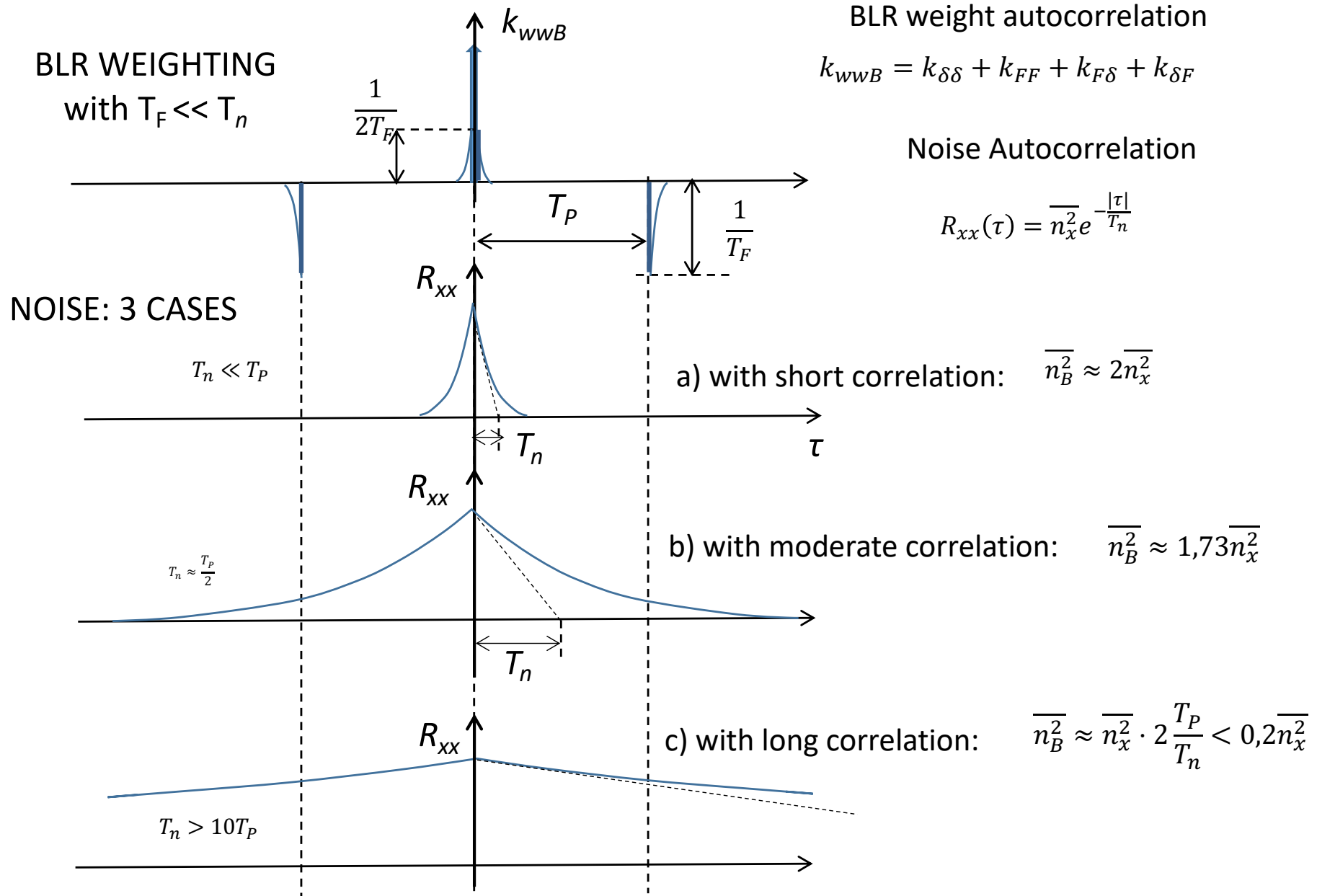
- with **moderate correlation time** (moderately wide band) the noise is enhanced:

with $T_n \approx \frac{T_P}{2}$ it is $\overline{n_B^2} \approx 1,73\overline{n_x^2}$

- only with **long correlation time** (low-frequency band) the noise is **attenuated***:

with $T_n > 10T_P$ it is $\overline{n_B^2} \approx \overline{n_x^2} \cdot 2\frac{T_P}{T_n} < 0,2\overline{n_x^2}$

 * note that anyway the level is **double** of that given by a simple CR filter with equal cutoff, that is with $T_F = RC = T_P$



BLR Filtering with slow differentiation

With T_F **NOT** negligible with respect to T_n , the effect on white noise depends also on the size of T_F compared to T_n and T_p . A long T_F can limit the white noise enhancement

$$\overline{n_B^2} = \overline{n_x^2} \left[1 + \frac{T_n}{T_n + T_F} \left(1 - 2e^{-\frac{T_p}{T_n}} \right) \right]$$

Let's evaluate how long must be T_F in the various cases of noise correlation

- with **short correlation time** $T_n \approx T_p / 10$ it is

$$\overline{n_B^2} \approx \overline{n_x^2} \left(1 + \frac{T_n}{T_n + T_F} \right)$$

for keeping $\overline{n_B^2} < 1,05 \overline{n_x^2}$ we need $T_F > 20 T_n \approx 2 T_p$

- with **moderate correlation time** $T_n \approx T_p / 2$ it is

$$\overline{n_B^2} \approx \overline{n_x^2} \left[1 + \frac{T_n}{T_n + T_F} \left(1 - \frac{2}{e^2} \right) \right] = \overline{n_x^2} \left[1 + 0,73 \frac{T_n}{T_n + T_F} \right]$$

for keeping $\overline{n_B^2} < 1,05 \overline{n_x^2}$ in this case we need $T_F > 7T_n = 3,5T_p$

BLR Filtering with slow differentiation

- with **long correlation time** $T_n > 10 T_p$ it is

$$\overline{n_B^2} \approx \overline{n_x^2} \left[1 - \frac{T_n}{T_n + T_F} \right] = \overline{n_x^2} \frac{T_F}{T_n + T_F}$$

No problem with such a low-frequency noise: it is attenuated by the BLR just as by a CR constant-parameter filter (with equal time constant $T_F = RC$)

The most interesting case for us is noise with moderate T_n . In fact, when the BLR works on the output of an optimum (or approximate-optimum) filter for wideband noise, the correlation time T_n and delay T_p are comparable, since they are both closely related to the band-limit of the signal pulse.

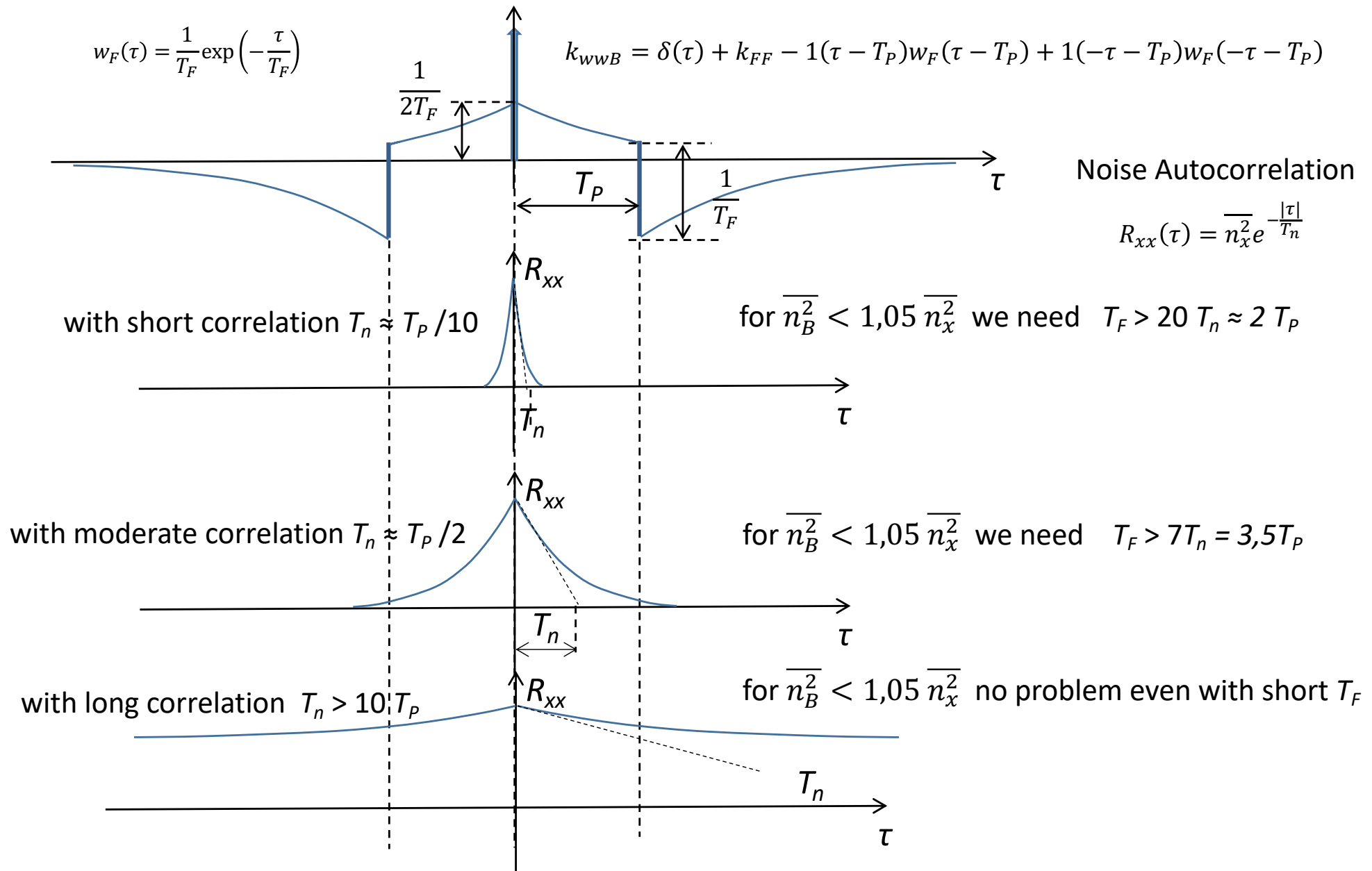
- We conclude that for avoiding enhancement of the white noise it is necessary to select a fairly slow BLR differentiation, i.e. a fairly long T_F

$$T_F \geq 5T_p$$

- This approach is satisfactory also for filtering the $1/f$ noise, notwithstanding that making T_F longer than T_p shifts down the BLR cutoff frequency, hence reduces the attenuation of $1/f$ noise. This is counterbalanced by the fact that the enhancement of $1/f$ noise at frequencies above the cutoff is limited by the low-pass filtering in the baseline subtraction, whereas with short T_F it is remarkable.

BLR Filtering with slow differentiation

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- The BLR is a high-pass filter that acts on noise and disturbances without affecting the pulse signal
- The BLR is a switched-parameter filter: the low-pass section within the high-pass filter structure is a boxcar integrator that acquires the baseline only in the intervals free from pulses
- The BLR can thus establish a high-pass band-limit at a high value (suitable for reducing efficiently the $1/f$ noise output power) without causing the signal loss suffered with a constant-parameter high-pass filter having the same band-limit
- The high-pass band-limit enforced by the BLR is given (with good approximation) by the low-pass bandlimit of the low-pass section in the BLR circuit structure
- The combination of: (1) optimum filter designed for the case of pulse signal in presence of wideband noise only (i.e. without $1/f$ noise) and (2) BLR specifically designed (for reducing the actual $1/f$ noise without worsening the wide-band noise) provides in most cases a quasi-optimum filtering solution.